

### Team #5

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### CE 4178 Highway Design and Construction

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#### **Team Member Contributions**

The proposed project is conducted and completed by the following team members. Corresponding tasks are listed below their names.

#### Ulrich Sounkoua

- Conducted the sight distance analysis and intersection sight distance analysis
- Evaluated roundabout design alternative using the GDOT ICE tool v2.14
- Evaluated the Road Diet alternative
- Report compilation and review

#### John Lyall

- Cost analysis and corresponding spreadsheets
  - ICE cost estimation tool for single-lane roundabout
  - GDOT pay items for road diet
- Report compilation/review and conclusion

#### Jermaine Jones Jr.

- Presenting alternative 1
- Constructed CAD drawings
  - Existing conditions
  - Alternatives

#### Jonathan Buttram

- Report compilation, review and quality checked it.
- Presentation compilation and review.
- Assisted in brainstorming alternative ideas for project.
- Presented on the alternative two topic, road dieting.

#### Juan Almanza

### **Abstract**

Throughout the design of a transportation project, many characteristics must be evaluated. Utilizing crash data, site distances, basic geometry and relevant topographic features are all important aspects to be considered. While mobility and drainage are large concerns on all roadways, ultimate safety yields the most important consideration. Resulting in numerous crashes from a sight distance issue, this study aims to justify a redesign of the intersection of Hammond Drive at Mount Vernon Highway, located in Sandy Springs, Georgia.

### Introduction

Located in the fifth largest city of Georgia, the Intersection of Hammond Drive at Mount Vernon Highway has been causing a lot of speeding issues recently and the issue has become one of the top priorities of the City of Sandy Springs Traffic Department. The current free right turn giving access to Hammond Drive coming from Mount Vernon Highway is one of the prime reasons that explains the speeding issue. Also, the EB traffic on Hammond Drive is faced with a high downsloping vertical curve that allows drivers to gain extra speed thus becoming a high crash hazard for anyone trying to make a left turn Mitchell Road and worse from Braemore Rd. Not only have Sandy Springs citizens have requested a design improvement, but the crash data provided below yields the fact that improvement is needed.

### Problem Statement and Objective

The primary goal of this project is to improve safety. In order to complete this, creating and researching two adequate solutions is the best route to take. The first solution is installing a mini roundabout at the current intersection of Hammond Dr and Mt Vernon Hwy to reduce speed. The second alternative is to implement a road diet that will include installing a protected left turn

at the intersection of Hammond Dr and Lake Forrest Dr. Lastly, alternative 3 is a "do nothing" approach to the problem.

### Methodology

In order to properly and effectively produce a solution, existing conditions must be studied in order to accomplish alternatives. This is carried out by conducting several measures such as: photos, survey, future impact analysis, future and current economic impacts, and safety research. After initial research is conducted, the next step is to utilize the GDOT ICE tool to determine whether a roundabout is feasible. As for the second alternative, using Synchro to evaluate the LOS before and after installing a protected left turn on Lake Forest Drive. Comparing the two options will be the final step in determining how to execute the challenge.

### **Existing Conditions**

The current state of Hammond Drive between Lake Forrest Drive and Mt Vernon Highway is inadequately designed for sight distance. The intersection of Hammond Drive @ Mt vernon Highway is signal controlled. An aerial image has been provided (Figure 1) to show the issue at a glance. Additionally, Figures 2-5 displays the issue from a driver perspective. Per crash data (Figure 7), many accidents happen while turning out of Mitchell Road NW and Braemore Drive NW. These crashes are mainly due to drivers not seeing each other. This issue is not only a mobility concern, but a safety problem for the present and future.



Fig. 1: Summary of issues



Fig. 2: Making a Left off Mitchell



Fig. 3: Making a Left off Braemore Drive NW



Fig. 4: Making a Right off Braemore Drive NW



Fig. 5: Sight Distance to the Left of Braemore



Fig. 6: Current Conditions (Created via Autodesk Infraworks.)

#### Crash Data

Criteria:

Agency: Sandy Springs Police Dept.

County: FULTON

Date of Collision is between 1/1/2014 and 12/31/2017

Roadway contains Hammond Dr, Sandy Springs Circle and Mt Vernon Hwy

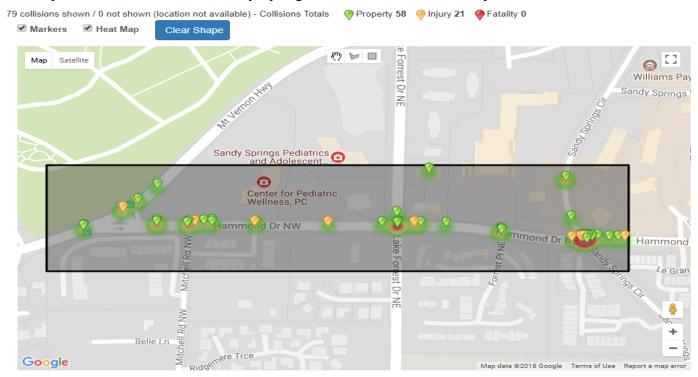


Fig. 7: Crash Data for Hammond Drive

Data Analysis - Intersection Sight Distance (ISD)

#### **AASHTO Standards**

### Design Intersection Sight Distance (Case B1 – Left turn from stop)

Speed (mph) *		Design Intersection Sight Distance (ft.)
25	155	280
30	200	335
35	250	390
40	305	445
45	360	500
50	425	555
55	495	610
60	570	665
65	645	720
70	730	775
75	820	830
80	910	885

Note: The distance shown is for a stopped passenger car to turn left onto a two-lane highway with no median and grades 3 percent or less.

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Figure#: Case B1

#### Case B1 Left Turn from Stop if the design vehicle is a passenger car.

ISD = 1.47\*Vmajor\*tg with Vmajor= 35mph tg= 7.5+0.5+0.8= 8.8  $\rightarrow$  ISD= 1.47(35 mph)(8.8s)= 452.76 ft> 390 ft required

#### Case B2 Right Turn from Stop if the design vehicle is a passenger car.

ISD=1.47\*Vmajor\*tg

 $tg=6.5+0.4=6.9 \rightarrow ISD=1.47(35 \text{ mph})(6.9s)=355 \text{ ft} > 335 \text{ required}$ 

Exhibit 9-57. Time Gap for Case B2—Right Turn from Stop and Case B3—Crossing Maneuver

	N	etric		US Customary					
Design speed (km/h)	Stopping sight distance (m)	Intersecti distand passeng Calculated (m)	ce for	Design speed (mph)	Stopping sight distance (ft)	Intersecti distand passeng Calculated (ft)	ce for		
20	20	36.1	40	15	80	143.3	145		
30	35	54.2	55	20	115	191.1	195		
40	50	72.3	75	25	155	238.9	240		
50	65	90.4	95	30	200	286.7	290		
60	85	108.4	110	35	250	334.4	335		
70	105	126.5	130	40	305	382.2	385		
80	130	144.6	145	45	360	430.0	430		
90	160	162.6	165	50	425	477.8	480		
100	185	180.7	185	55	495	525.5	530		
110	220	198.8	200	60	570	573.3	575		
120	250	216.8	220	65	645	621.1	625		
130	285	234.9	235	70	730	668.9	670		
				75	820	716.6	720		
				80	910	764.4	765		

Note: Intersection sight distance shown is for a stopped passenger car to turn right onto or cross a two-lane highway with no median and grades 3 percent or less. For other conditions, the time gap must be adjusted and required sight distance recalculated.

Figure#: Case B2

#### Case 3 does not apply as we have a T-intersection.

#### Sight Distance

The minimum Stopping Sight Distance (SSD) is 250' for a grade of 3% but given that we have a sagging curve with a grade of about 8%-10% we should have a greater sight distance. The Sight Distance to the Right (SDR) is adequate in this case.

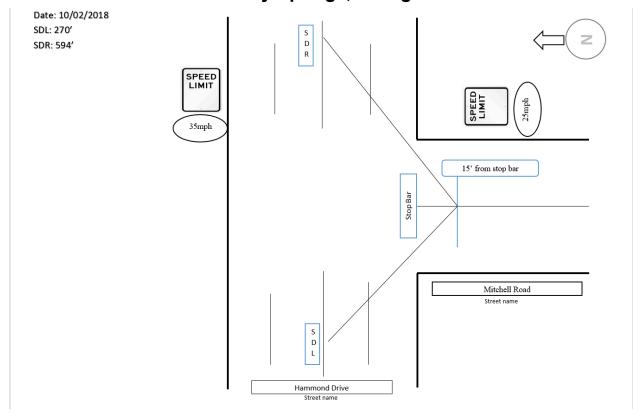


Figure 8: Site distance from Mitchell Road



#### 3E SIGHT DISTANCE-without medians

Driveways should be located to provide adequate sight distance. Minimum intersection sight distance criteria are provided in Table 3-4. The line of sight establishes the boundary of a sight triangle, within which there should be no sight obstruction.

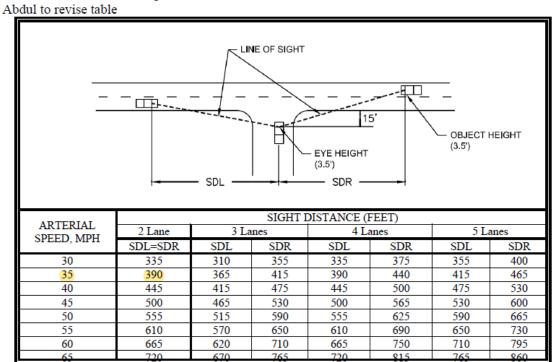
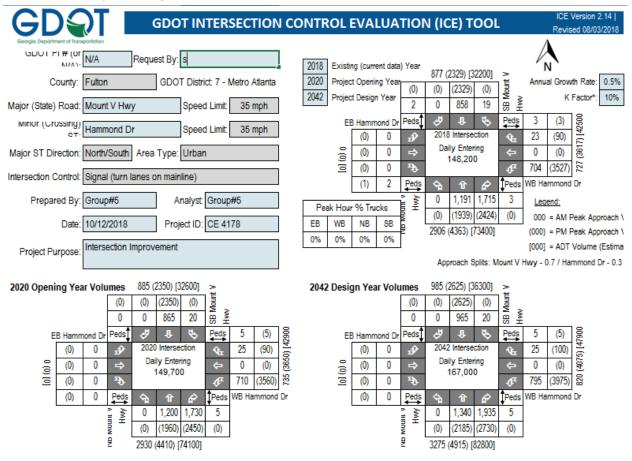


Figure 9: Adequate site distance illustration.

The measured sight distance to the left (SDL) is 270 ft <390 ft required  $\rightarrow$  Not adequate. The measured SDR is adequate.

### **Analysis**

Alternative analysis using the GDOT ICE tool V2.14



Existing Year Volume	EB H	ammor	nd Dr	WB H	lammo	nd Dr	NB M	ount V	Hwy	SB Mount V Hwy			
Inputs	LT	TH	RT	LT	TH	RT	LT	TH	RT	LT	TH	RT	
AM Peak Hour:	0	0	0	704	0	23	0	1,191	1,715	19	858	0	
PM Peak Hour:	Hour: (0) (0) (0)		(3527) (0) (90)		(0) (1939) (2424			(0) (2329)		(0)			
	Ea	stbou	nd	Westbound			Northbound			Southbound			
Peak Hour Truck %:		0.0%			0.0%			0.1%			0.3%		
AM (PM) Ped X-ings:	2	(1)		3	(3)		3 (0)			2 (0)			

<sup>\*</sup> K Factor = proportion of annual average daily traffic occurring in the peak hour

Open Yr Vol	ume Override	EB Hammond Dr						NB Mount V Hwy			SB Mount V Hwy		
		LT	TH	RT	LT	TH	RT	LT	TH	RT	LT	TH	RT
	AM Peak Hour:	0	0	0	0	0	0	0	0	0	0	0	0
	PM Peak Hour:	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)
AM	(PM) Ped X-ings:	0	(0)		0	(0)		0	(0)		0	(0)	

Design Yr V	olume Override	EB Hammond Dr			WB Hammond Dr			NB Mount V Hwy			SB Mount V Hwy		
		LT	TH	RT	LT	TH	RT	LT	TH	RT	LT	TH	RT
	AM Peak Hour:	0	0	0	0	0	0	0	0	0	0	0	0
	PM Peak Hour:	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)
AM	(PM) Ped X-ings:	0	(0)		0	(0)		0	(0)		0	(0)	

ADT Volume	Override	Exist	Open	Desig
		Year	Year	n
	EB Hammond Dr	0	0	0
	WB Hammond Dr	0	0	0
	NB Mount V Hwy	0	0	0
	SB Mount V Hwy	0	0	0

G	GDQT GDOT ICE STAGE 1: SCREENING DECISION RECORD												
Georgia I	Department of Transportati	00		<u></u>			DECIS			ICE Version 2.14   Revised 08/03/2018			
Proje Prepa Analy Date: Ans eac si Reco	wer "Yes" or ch control typ hould be eval ord; enter just rsection Alte	N/A  Mount V Hwy @ Hammond Dr  Group#5  Group#5  10/12/2018  "No" to each policy question for e to identify which alternatives uated in the Stage 2 Decision in the rightmost column reative (see "Intersections" tab for n of intersection/interchange type)	Note: I may be evaluat Stage fewer a evaluat	Up to 5 all a selected ded; Use to scree alternative de in Stag	ternatives and his ICE n 5 or es to e 2	THE STATE OF THE S	S. John S. Joh	Control of the state of the sta		of the state of th			
	T .	al (Minor Stop)	No	No	No	No	No	No	No				
	Conventions	al (All-Way Stop)	No	No	No	No	No	No	No				
	Mini Rounda	about	Yes	Yes	Yes	Yes	Yes	Yes	Yes	<b>T</b>			
	Single Lane	Roundabout	Yes	Yes	Yes	Yes	Yes	Yes	Yes				
suo	Multilane Ro	undabout	No	No	No	No	No	No	No				
rsect	RCUT (stop	control)	No	No	No	No	No	No	No				
Unsignalized Intersections	RIRO w/dov	vn stream U-Turn	No	No	No	No	No	No	No				
nalize	High-T (uns	ignalized)	No	No	No	No	No	No	No				
Jnsig	Offset-T Inter	rsections	No	No	No	No	No	No	No				
	Diamond Inte	erch (Stop Control)	No	No	No	No	No	No	No				
	Diamond Inte	erch (RAB Control)	No	No	No	No	No	No	No	ROW restrictions			
	No LT Lane In No RT Lane I		No	No	No	No	No	No	No				
	Other unigna	alized (provide description):	No	No	No	No	No	No	No				
	Traffic Signa	ı	No	No	No	No	No	No	No	Existing			
	Median U-T	urn (Indirect Left)	No	No	No	No	No	No	No				
	RCUT (signa	alized)	No	No	No	No	No	No	No				
		nt Turn (CFI)	No	No	No	No	No	No	No				
ions	Continuous (		No	No	No	No	No	No	No				
ersect	Jughandle		No	No	No	No	No	No	No				
alized Intersections	Quadrant Ro	padway	No	No	No	No	No	No	No				
		erch (Signal Control)	No	No	No	No	No	No	No				
Sign	Diverging Di		No	No	No	No	No	No	No				
	Single Point		No	No	No	No	No	No	No				
	No LT Lane In	nprovements	No	No	No	No	No	No	No				
	No RT Lane In Other Signali	reprovements ized (provide description):	No	No	No	No	No	No	No				
	J												

<sup>=</sup> Intersection type selected for more detailed analysis in Stage 2 Alternative Selection Decision Record

GDQT	GDOT IC	E STAGE	2: A	LTERNATI	VE	SELECTION DEC	ISION R	ECORD		
Georgia Department of Transportation								ICE Version	2.14   Revised	08/03/2018
GDOT PI # (or N/A)	N/A		GDOT District: 7 - Metro Atlanta					Date:	10/12/2018	
County:	Fulton			Area Type	1	Urban	Age	ency/Firm:	Group#5	
Project Location:				Analyst:	Group#5					
Existing Intersection Control:	ne)		Type of Analysis:	Safety Fur	nded Projec	t				
Opening / Design Year Traffic Operations						crash Data: Enter 5 most recent years of intersection	С	rash Seven	ty	
Intersection meets signal/AWS warrants?	None			Complete Streets		crash data	PDO	Injury Crash*	Fatal Crash*	
Traffic Analysis Measure of Effectiveness	Intersecti	on Delay	Warrants Met?			Angle	0	0	0	#DIV/0!
Traffic Analysis Software Used	selec	t one	<b>~</b>	PEDESTRIANS	əd	Head-On	0	0	0	#DIV/0!
Analysis Time Period	AM Peak Hr	PM Peak Hr	<b>~</b>	BICYCLES	5 TV	Rear End	0	0	0	#DIV/0!
2020 Opening Yr No-Build Peak Hr Intersection	0.0 sec	0.0 sec	<b>~</b>	TRANSIT	rasi	Sideswipe - same	0	0	0	#DIV/0!
2020 Opening Yr No-Build Peak Hr Intersection V/C	0.00	0.00			0	Sideswipe - opposite	0	0	0	#DIV/0!
2042 Design Yr No-Build Peak Hr Intersection Delay				Not Collision w/Motor Veh	0	0	0	#DIV/0!		
2042 Design Yr No-Build Peak Hr Intersection V/C				TOTALS:	0	0	0	0		
						* Number of crashes resulting	in injuries / fat	talities, not numb	er of persons	

Alternatives Analysis:	Alterna	ative 1	Altern	ative 2	Alternative 3	Alternative 4	Alternative 5
Proposed Control Type/Improvement:	Mini Rou	ndabout		Lane dabout	N/A	N/A	N/A
Project Cost: (From CostEst Worksheet)	Additional de.	scription here		scription here			
Construction Cost	\$90.	000	\$479	000			
ROW Cost	\$377.000		\$966	·			
Environmental Cost	\$377 \$1	,		0			
		-					
Reimbursable Utility Cost		\$3,000		,000			
Design & Contingency Cost	\$33,000		\$133	,000			
Cost Adjustment (justification req'd)				%			
Total Cost	\$503,000		\$1,592,000				
Traffic Operations:							
Traffic Analysis Software Used	selec	t one	select one				
Analysis Period	AM Peak Hr	PM Peak Hr	AM Peak Hr PM Peak Hr				
2042 Design Yr Build Intersection Delay	0.0 sec	0.0 sec	0.0 sec	0.0 sec			
2042 Design Yr Build Intersection V/C	0.00	0.00	0.00	0.00			
Safety Analysis:							
Predefined CRF: PDO	#N	/A	24	1%			
Predefined CRF: Fatal/Inj	#N	/A	71	1%			
Predefined CRF Source:				inghouse #s 4255			
User Defined CRF: PDO							
User Defined CRF: Fatal/Inj							
User Defined CRF Source							
(write in if applicable):							

				i .	i
Environmental Impacts:1			_		
Historic District/Property	None	None	<b>-</b>		
Archaeology Resources	None	None			
Graveyard	Significant	None			
Stream	None	None			
Underground Tank/Hazmat	None	None			
Park Land	None	None			
EJ Community	None	None			
Wooded Area	Minimal	None			
Wetland	None	None			
Stakeholder Posture:	I. '			nn t jeopardise project delive nact documentation will be in	-
Local Community Support	Strong	Strong			
GDOT Support	Neutral	Neutral			
	115.11.6		1	T	
Final ICE Stage 2 Score:	#N/A	2.2			
Rank of Control Type Alternatives:	#N/A	#N/A			
	Note: Stage 2 score is not give	ven (shown as "-") if signal or	AWS is selected as control ty	pe but respective warrants are	not met
Provide additional comments and/or					
explain any unique analysis inputs, or					
results (as necessary):					
Table (as necessary).					

The single lane roundabout resulted in a score of 2.2 while a mini-roundabout is not feasible due to environmental issues. Thus, the mini-roundabout should no longer be considered a viable option.

#### Alternative #1

The first alternative is to design a single lane roundabout at the current intersection of Hammond Drive and Mt Vernon Highway.



Figure 10: Roundabout model for Alternative 1 (Created via Autodesk InfraWorks)

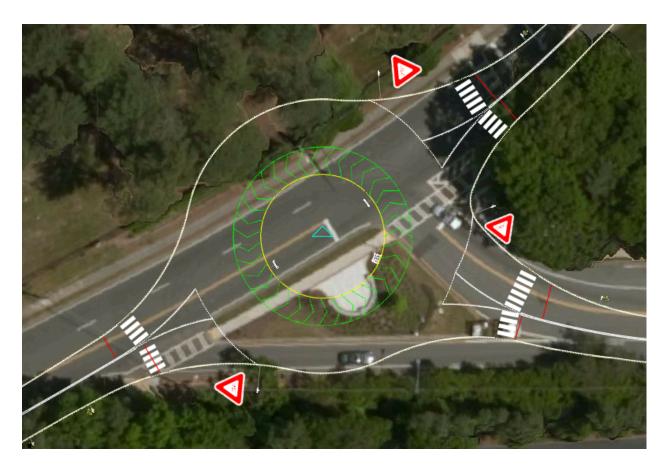


Figure 11: Roundabout design overlaying the current design of Mt Vernon Hwy and Hammond Dr. (Created via Autodesk Infraworks and exported to Autodesk Civil 3D)

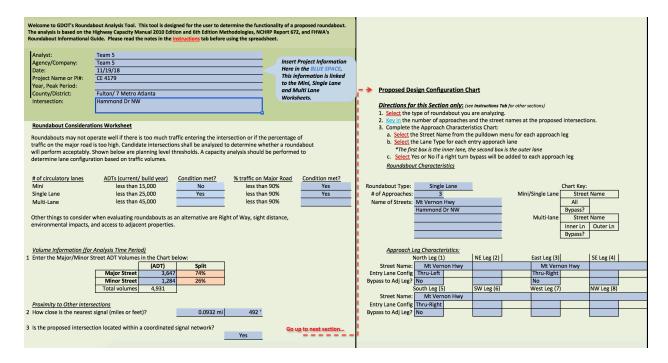


Figure #. GDOT's Roundabout Analysis Tool

**Table 1: Single Lane Roundabout vehicle flow information** 

	Result	s: Approa	ch Measu	res of Effe	ectivenes	s		
HCM 6th Edition	N	NE	E	SE	S	SW	W	NW
Entry Capacity, vph	362	NA	421	NA	NA	115	NA	NA
Entry Flow Rates, vph	1126	NA	1352	NA	NA	2713	NA	NA
V/C ratio	3.11		3.21			23.63		
Control Delay, sec/pcu	979		1021			10252		
LOS	F		F			F		
95th % Queue (ft)	2494		3014			8196		
Notes:								v 4.0
						Unit Legen	id:	
						vph = vehi	cles per hou	r
						PHF = peal	k hour facto	r
						F <sub>HV</sub> = heav	y vehicle fac	ctor
						pcu = pass	enger car ur	nit

Using the GDOT Roundabout Analysis Tool V4.1 it has been found that placing a Mini Roundabout or a Single Lane Roundabout would lead to a LOS (F). The existing LOS is B therefore a Single Lane Roundabout or Mini Roundabout would not be a better alternative to the existing intersection.

### Cost Analysis: Single Lane Roundabout

 Project Information
 Location:
 Mount V Hwy @ Hammond Dr
 County:
 Fulton
 Date:
 10/12/2018

 GDOT PI # (or N/A):
 N/A
 Area Type:
 Urban
 Agency/Firm:
 Group#5

 Existing Intersection Control:
 Signal (turn lanes on mainlin)
 GDOT District:
 7 - Metro Atlanta
 Analyst:
 Group#5

Type of Analysis: Conventional Non-Safety Funded Project Major Street Direction: North/South

Table 1: Existing Conditions	NE	NB Mount V Hwy			B Mount V H	wy	EE	3 Hammond	Dr	WB Hammond Dr			
Movement	Left Turn	Thru	Right Turn	Left Turn	Thru	Right Turn	Left Turn	Thru	Right Turn	Left Turn	Thru	Right Turn	
Number of Lanes	0	1	1	1	1	0	0	0	0	1	0	1	
Lane Widths*	0'	12'	12'	12'	12'	0'	0'	0'	0'	12'	0'	12'	
Bay Length**	0'		0'	110'		0'	0'		0'	0'		0'	
Median Width		0'			0'			0'			0'		
Right-of-Way			2	4'					3	0'			

	Single Lane										
Table 2: Proposed Conditions	Roundabout	N/A	N/A	N/A	N/A	Site Context		<u>l</u>	ntersections		
Proposed Pavement Type	F.D. Asphalt	None	None	None	None	Topography:	Le	vel	Signal Poles	Mast Arm	
Reimbursable Utility:	Moderate	Moderate	Moderate	Moderate	Moderate	Traffic Mgmt Plan:	Maintai	n Traffic De	esign Vehicle	WB-67	
# of Driveway(s) Impacted	0	0	0	0	0	Project Size:	Single Int	tersection Existing	Interchange?	No	
Modify/Replace Traffic Signal	2	0	0	0	0	_		<u>R</u>	oundabouts		
Lighting Poles (ea)	0	0	0	0	0			Inscrib	ed DIA - Mini		
Flashing Beacons (ea)	0	0	0	0	0	Cost Multipliers		Inscribed DIA - Single			
RFB/PHB Ped Crossings (ea)	3	0	0	0	0	Grading Complete:	15%	Inscribe	ed DIA - Multi		
New/Replace Sidewalks (LF)	450'	0'	0'	0'	0'	Reimbursable Utility:	5%	Circulatin	g Lane Width	12	
New/Replace Cross Drains (LF)	0'	0'	0'	0'	0'	Traffic Control:	20%	ROW Costs	•		
New/Replace Guardrail (LF)	0'	0'	0'	0'	0'	Project Size:	0%	Prevalent ROW Type:	Mixed (A	Average)	
New Retaining Wall (LF)	0'	0'	0'	0'	0'	Prelim Engineering:	15%	ROW Cost/Acre:	\$1,02	8,213	
Bridge:New/Widen/Replace (sqft)	0	0	0	0	0	Project Contingency:	20%	ROW Multiplier:	1.	.6	
Add'l ROW/Easements/Demolition	\$134,696	\$0	\$0	\$0	\$0	_					

Table 3: Control Type Cost Breakdown

	Per Ln Mi		Single Lane	Roundabout	N	/A	N/	/A	N	/A	N/	Α
Pay Item	Unit Cost	Unit Cost	Quantity	Cost	Quantity	Cost	Quantity	Cost	Quantity	Cost	Quantity	Cost
New Construction (Base & Pave)	\$500K/LM	\$9.47/sqft	19,672	\$322,088	#N/A	#N/A						
Roadway Mill and Overlay	\$64K/LM	\$1.21/sqft	0	\$0	#N/A	#N/A						
Urban C&G/Drainage - both sides	441-6720	\$19.08/LF	2000	\$65,979	#N/A	#N/A						
Rural Typ Drainage - both sides	\$150K/LM	\$2.84/LF	0	\$0	#N/A	#N/A						
Concrete Island (sqyd)	n/a	\$51.58/syd	360	\$32,105	#N/A	#N/A						
Median Landscaping	\$100K/LM	\$1.89/LF	3000	\$9,824	#N/A	#N/A						
Typical Driveways Impacted (ea)	n/a	\$7,500 ea	0	\$0	#N/A	#N/A						
Typical E&S Control Temp/Perm	\$150K/LM	\$34.09/LF	1000	\$45,341	#N/A	#N/A						
Roundabout Truck Apron (sqft)	n/a	\$10.25/sqft	4776	\$84,633	#N/A	#N/A						
Signing & Marking	<b>\$</b> 0	\$22.73/LF	1,000	\$30,231	#N/A	#N/A						
Flashing Beacon (ea)	n/a	\$20,000 ea	0	\$0	#N/A	#N/A						
New Traffic Signal (Mast Arms)	674-1000	\$182,575ea	2	\$485,650	#N/A	#N/A						
Lighting (per pole)	n/a	\$5,607 ea	0	\$0	#N/A	#N/A						
Signalized Ped Crossings (ea)	n/a	\$19,637 ea	3	\$78,352	#N/A	#N/A						
6' Sidewalk (LF)	n/a	\$49.23/LF	450	\$29,464	#N/A	#N/A						
New/replace cross drains (LF)	n/a	\$41.31/LF	0	\$0	#N/A	#N/A						
Typical Guardrail (LF)	n/a	\$65.56/LF	0	\$0	#N/A	#N/A						
Retaining Wall (LF)	n/a	\$808.52/LF	0	\$0	#N/A	#N/A						
Bridge widen/replace (SF)	n/a	\$210/sqft	0	\$0	#N/A	#N/A						
Env Costs (from Stage 2 impacts)	n/a	n/a	0	\$0	#N/A	#N/A						
Grading Complete - 15%	n/a	n/a		\$354,212		#N/A						
Traffic Control - 20%	n/a	n/a		\$314,855		#N/A						
Reimbrusable Utility	n/a	n/a		\$59,183		#N/A						
Preliminary Engineering - 15%	n/a	n/a		\$236,141		#N/A						
Contigency - 20%	n/a	n/a		\$314,855		#N/A						
ROW Cost/Acre: Mixed (Average)	n/a	#########		\$301,194		#N/A						
Add'l ROW / Displacement / Demo	n/a	n/a		\$134,696		#N/A						
ROW Multiplier - 1.6	n/a	n/a		\$261,534		#N/A						
Project Scale Reduction - 0.0%	n/a	n/a		\$0		#N/A						
Grand Total Costs				\$3,160,000		#N/A						

Table 2: Cost Analysis for Alternative 1

#### Alternative #2

The second alternative is to implement a road diet and a protected left turn at the intersection of Hammond Drive and Lake Forrest Drive.





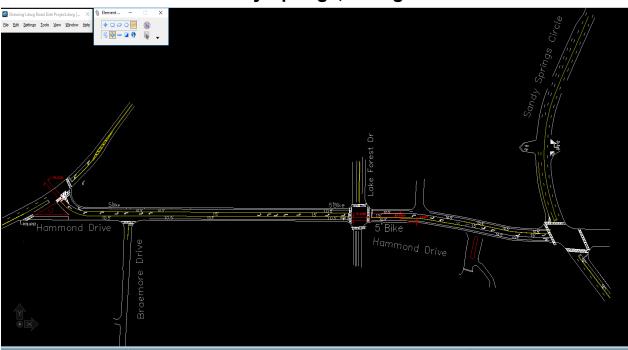


Table 2: Left Turn warrant analysis for Lake Forrest Dr @ Hammond Dr

		Vol	ume	Cross P	roduct
Intersection	Movement	AM Peak Hour	PM Peak Hour	AM Peak Hour	PM Peak Hour
	EBTH	582	621	36,666	47,817
	WBL	126	154	30,000	47,017
	WBTH	219	611	438	2,444
Hammond Dr. and Lake Forrest Dr.	EBL	4	8	430	2,777
Hammond Dr. and Lake Forrest Dr.	NBTH	150	187	375	7,480
	SBL	5	80	373	7,400
	SBTH	254	192	8,255	7,584
	NBL	65	79	6,233	7,30+

Leading left turn phase = 125 VPH or crossproduct of 50,000 VPH

Leading left turn phase denoted by:

Lagging left turn phase = 75 VPH or crossproduct of 30,000 VPH

Lagging left turn phase denoted by:

#### NOTE:

The AM Peak Hour is 7:45 AM to 8:45 AM and PM Peak Hour is 5:00 PM to 6:00 PM

The total Peak Hour Volumes are summed across the 4 15 minute intervals

Table 3: AM

	Delay (Sec)	LOS	Approach LOS	Approach delay
NBL	15.4	В		
NBT	0.0	-	Α	9.2
NBR	12.9	В		
SBL	14.0	В		
SBT	0.0	-	В	10.3
SBR	12.8	В		
EBL	17.4	В		
EBT	0.0	-	С	23.4
EBR	17.7	В		
WBL	15.4	С		
WBT	0.0	-	С	24.7
WBR	12.9	В		
Intersection				
mersection	16.6		В	

Table 4: PM

	Delay (Sec)	LOS	Approach LOS	Approach delay
NBL	0.8	Α		
NBT	0.0	-	В	14.1
NBR	0.8	Α		
SBL	1.0	Α		
SBT	0.0	-	В	13.7
SBR	0.6	Α		
EBL	15.0	В		
EBT	0.0	-	В	16.4
EBR	15.2	В		
WBL	37.0	D		
WBT	0.0	-	D	36.4
WBR	18.5	В		
Intersection	14.3		В	

**Table 6: PM-LEFT TURN** 

	Delay (Sec)	LOS	Approach LOS	Approach delay
NBL	11.0	В		
NBT	0.0	-		
NBR	10.2	В		
SBL	13.8	В		
SBT	0.0	-		
SBR	8.8	Α		
EBL	18.2	В		
EBT	0.0	-		
EBR	85.6	F		
WBL	41.5	D		
WBT	0.0	-		
WBR	28.5	С		
Intersection	41.6		D	

**Table 7: AM LEFT TURN** 

	Delay (Sec)	LOS	Approach LOS	Approach delay
NBL	11.3	В		
NBT	0.0	-	В	20.1
NBR	9.1	Α		
SBL	10.3	В		
SBT	0.0	-	С	19.4
SBR	9.1	Α		
EBL	15.5	В		
EBT	0.0	-	С	80.4
EBR	69.0	F		
WBL	26.8	С		
WBT	0.0	-	В	30.2
WBR	15.4	В		
Intersection	36.2		D	

**Table 8: FINAL SHEET** 

### **Intersection Capacity Analysis**

		_															
lake on a skin o	Approach/				Exis	ting				Protected Left turn							
Intersection	Movement			AM Peak				PM Peak		AM Peak				PM Peak			
		Delay	LOS	Approach delay	Approach LOS	Delay	LOS	Approach delay	Approach LOS	Delay	LOS	Approach delay	Approach LOS	Delay	LOS	Approach delay	Approach LOS
	NBL	15.4	В			0.8	A			11.3	В			11.0	В		
	NBT	0.0		9.2	A	0.0		В	14.1	0.0		В	20.1	0.0			
	NBR	12.9	В			0.8	A			9.1	A			10.2	В		
	SBL	14.0	В			1.0	A			10.3	В			13.8	В		
	SBT	0.0		10.3	В	0.0		В	13.7	0.0		С	19.4	0.0	٠		
Hammond Drive @ Lake Forrest	SBR	12.8	В			0.6	A			9.1	A			8.8	A		
	EBL	17.4	В			15.0	В			15.5	В			18.2	В		
	EBT	0.0	٠	23.4	C	0.0	-	В	16.4	0.0		C	80.4	0.0			
	EBR	17.7	В			15.2	В			69.0	F			85.6	F		
	WBL	15.4	С			37.0	D			26.8	С			41.5	D		
	WBT	0.0		24.7	С	0.0		D	36.4	0.0		В	30.2	0.0			
	WBR	12.9	В			18.5	В			15.4	В			28.5	C		
	Overall			16.6	В			14.3	В			36.2	D			41.6	D

Analyzing the results in the table above, it is noticed that the LOS after the installation of a protected left turn is D while the existing LOS is B. It can be concluded that the road diet with a protected left-turn is not a practical or recommended solution to implement. However, giving that the traffic volume on the eastbound left turn is really small implementing a permissive left turn for the EBLT and a Protected and Permissive for the WBLT would solve the delay issue.

### Cost Analysis: Road Diet

The following cost analysis was performed using the Georgia Department of Transportation Item Mean Summary from January 2013.

Table 9: Cost Analysis of Alternative #2

Item Code	Item Description	Quantity	UM	Uni	t Cost	Tot	tal Cost
153-1300	FIELD ENGINEERS OFFICE TP 3	1	EA	\$	2,251.10	\$	2,251.10
652-0094	PAVEMENT MARKING, SYMBOL, TP 4	4	EA	\$	50.09	\$	200.36
652-0110	PAVEMENT MARKING, ARROW, TP 1	4	EA	\$	50.24	\$	200.96
652-0120	PAVEMENT MARKING, ARROW, TP 2	7	EA	\$	49.50	\$	346.50
652-2501	SOLID TRAFFIC STRIPE, 5 IN, WHITE	0.193	LM	\$	379.51	\$	73.25
652-2502	SOLID TRAFFIC STRIPE, 5 IN, YELLOW	0.432	LM	\$	383.10	\$	165.50
652-3501	SKIP TRAFFIC STRIPE, 5 IN, WHITE	0.019	LM	\$	281.57	\$	5.35
652-3502	SKIP TRAFFIC STRIPE, 5 IN, YELLOW	0.432	GLM	\$	252.90	\$	109.25
652-5701	SOLID TRAFSTRIPE, 24 IN, WHITE	10	LF	\$	2.03	\$	20.30
653-0220	THERMOPLASTIC PVMT MARKING, WORD, TP	1	EA	\$	87.50	\$	87.50
656-5000	REMOVE EXIST TRAF MARKINGS-	2	EA	\$	16.00	\$	32.00
					Σ	\$	3,492.07

### **Pavement Design**

Using the GDOT Pavement Design Tool v2.0 the following pavement dimensions were obtained for a Full-Depth Flexible Pavement Design.

**Table 10: Flexible Pavement Design Analysis** 

	Flexible Pa	vement Desig	gn Analysis
PI Number	0004178	County(s)	Cobb
Project Number		Design Name	Group 5
Project Description	Polytechnic Lane		

	Т	raffic Data (AADTs a	re one-wa	ıy)		Miscellaneous Data			
Initial Design Year	2018	Initial AADT, VPD	4,931	24 Hour Truck %	1.00	Lanes in one direction	2		
Final Design Year	2038	Final AADT, VPD	7,000	SU Truck %	0.00	Curb & Gutter/Barrier	No		
		Mean AADT, VPD	5,966	MU Truck %	1.00				

		Design Data			Part State
Lane Distribution Factor (%) 74.00		Soil Support Value	2.00	Single Unit ESAL	0.40
Terminal Serviceability Index 2.50		Regional Factor	1.80	Multiple Unit ESAL	2.00
		User Defined 18-KIP ESAL	0.00	Calculated 18-KIP ESAL	2.00
Non-Standard Value Comment					

Design Loading (Calculated 18-KIP ESAL)					
Mean AADT, VPD	LDF (%)	Vehicle Type	Volume (%)	ESAL Factor	Daily ESAL
	74.00	Single Unit Truck	0.00	0.40	0
5,966		Multi Unit Truck	1.00	2.00	89
				Total Daily ESALs	89
			Total	Design Period ESALs	649,700

Proposed Flexible Full Depth Pavement Structure					
Course	Material	Thickness (inches)	Structural Coefficient	Structural Value	
Course 1	12.5 mm Superpave	2.50	0.4400	1.10	
Course 2		2.00	0.4400	0.88	
	19 mm Superpave	1.00	0.3000	0.30	
Course 3	25 mm Superpave	3.50	0.3000	1.05	
Course 4	Graded Aggregate Base	7.00	0.1600	1.12	
Required S	N 4.61 Proposed pavement is 3.53% Und	lerdesigned	Proposed SN	4.45	

Table 11: Criteria For Use of Asphaltic Concrete Layer and Mix Types

CRITERIA FOR USE OF ASPHALTIC CONCRETE LAYER AND MIX TYPES (Using Base Year Two-Way ADT)

	4	Base Year Two-Way		LAYER THICKNESS AND/OR SPREAD RATE Customary, (Metric)				
	PAY ITEM	ADT	MIX TYPE	(Minimum)	USE	(Maximum)	REMARKS	
Drainage	400-3206	>25,000	12.5 mm OGFC	85 lbs/yd², (47 kg/m²)	90 lbs/yd <sup>2</sup> , (50 kg/m <sup>2</sup> )	95 lbs/yd², (53 kg/m²)	For High ADT State Routes with speed limits ≥ 55 mph.	
	400-3624	N/A	12.5 mm PEM	110 lbs/yd², (60 kg/m²)	135 lbs/yd², (75 kg/m²)	165 lbs/yd², (90 kg/m²)	For Interstate Routes.	
	402-3814	<800		3/4",	<sup>7</sup> / <sub>8</sub> ", 90 lbs/yd <sup>2</sup> , (22 mm, 50 kg/m <sup>2</sup> )	1- <sup>1</sup> / <sub>8</sub> ", 125 lbs/yd <sup>2</sup> , (28 mm, 70 kg/m <sup>2</sup> )	For State and Off-system Routes with low truck traffic volume (< 100 trucks per day).	
	402-3816	800 to 1000	4.75 mm	85 lbs/yd², (19 mm, 45 kg/m²) (2				
	402-3100	<800	9.5 mm	<sup>7</sup> / <sub>8</sub> ", 90 lbs/yd <sup>2</sup> ,	1-¼"*, 1-¼", 135 lbs/yd², 135 lbs/yd²,	1-¼", 135 lbs/yd²,	For State and Off-system Routes  * For Off-system Routes only USE: 1-1/8", 125 lbs/yd², (28 mm, 70 kg/m²)	
Surface**	402-3101	800 to 2000	Type I Superpave		(32 mm, 75 kg/m²)	(32 mm, 75 kg/m²)		
	402-3102	2000 to 4000	9.5 mm	125 lbs/vd² 13	1-¼", 135 lbs/vd².	1-¼", 135 lbs/yd², (32 mm, 75 kg/m²) 1-½", 165 lbs/yd², (38 mm, 90 kg/m²)	For State and Off-system Routes.	
	402-3103	4000 to 10,000	Type II Superpave					
	402-3130	10,000 to 25,000	12.5 mm Superpave	1- <sup>3</sup> / <sub>8</sub> ", 150 lbs/yd², (35mm, 80 kg/m²)	1-½", 165 lbs/yd², (38 mm, 90 kg/m²)	2-½", 275 lbs/yd², (64 mm, 150 kg/m²)	For State Routes and for shoulders of Interstate Routes	
	402-4510	25,000 to 50,000	12.5 mm Superpave w/polymer Modified AC	1-3/8", 150 lbs/yd², (35mm, 80 kg/m²)	1-½", 165 lbs/yd², (38 mm, 90 kg/m²)	2-½", 275 lbs/yd², (64 mm, 150 kg/m²)	For High ADT State Routes, all Interstate Routes; an Interstate Ramps.	
	402-3600	>50,000	12.5 mm SMA	1- <sup>3</sup> / <sub>8</sub> ", 150 lbs/yd <sup>2</sup> , (35mm, 80 kg/m <sup>2</sup> )	1-½", 165 lbs/yd², (38 mm, 90 kg/m²)	3", 330 lbs/yd², (75mm, 180 kg/m²)	For Interstate Routes and for State Routes when recommended by OMR.  OMR may recommend 2-inch lift 12.5 mm SMA on Interstates.	

#### 2.4 Flexible Pavement

**Note:** The project location determines base layer selection.

#### 2.4.1 Graded Aggregate Base Layers

GAB can be placed in a single layer or multiple layers depending upon its thickness; layers not to exceed 8 inches and not to exceed 2 layers. Layer Coefficients may be in the range of 0.12 to 0.16

**Figure 12: GDOT Pavement Design Manual** 

**Table 13: Earthworks Using Pavement Design** 

Roundabout Radius	Roundabout Area		
50 ft.	907.92 Cu. Yd		

Course	Volume (Cu.Yd)
Surface	68.09
Base	81.71
Subbase	95.33
Subgrade	190.66
Total	435.79

### Alternative #3 Do Nothing

This alternative is explained below in the conclusion.

### Conclusion

Sandy Springs, Georgia is an area that is ever growing and will always need improvements. Safety, mobility, and cost effectiveness are all important considerations when improving traffic flow. Due to the fact that there have been numerous accounts from citizens complaining about the sight distance issue on Hammond Drive, a redesign is necessary. All of the alternatives for this project present many positives and negatives, which need to be considered.

The first alternative includes designing a single-lane roundabout to reduce the speed of oncoming traffic to Hammond Drive. The design promotes safety and appearance, but lacks heavily in cost effectiveness. Noting that the cost of the roundabout would be over \$2M and the traffic that would result during construction, conclusively deem this design inefficient.

The third option consists of doing nothing. While this is the cheapest cost, it does not necessarily improve safety or mobility. This option could prove viable in a sense that it wouldn't hurt or set back anything, however it could risk more potential crashes.

The second alternative consists of a road diet spanning across Hammond Drive. Taking AASHTO Standards into consideration, this design is the most viable. Accidents would be reduced and traffic mobility would be greatly improved. The relatively low construction and maintenance cost while improving safety conclusively justifies this design.

### References

-Georgene M. Geary, P.E., State Materials and Research Engineer, "Pavement Design", DEPARTMENT OF TRANSPORTATION STATE OF GEORGIA, March 18, 2011

-"GDOT Pavement Design Tool User Guide", Georgia Department of Transportation Office of Design Policy and Support Engineering Support & Services, July 15, 2013

-AASHTO "7th Edition Highway & Street Design "Green Book"", 2018

-"GDOT Pavement Design Manual", *Georgia Department Office of Materials and Research*, December 6,2005

### **Appendix**



#### INTERSECTION CONTROL TYPE DESCRIPTIONS

Click on intersection images for additional resource publications

ICE Version 2.14 | Revised 08/03/2018

#### **Unsignalized At-Grade Intersections**



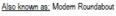
Conventional Minor Street or All-Way Stop: At minor street stop (2-way stop) intersections, vehicles on minor street stop and give right-of-way to major street. At all-way stop (AWS) intersections, all vehicles must stop and take turns entering the intersection. Both (4-leg) intersection types have 32 baseline conflict points and have limited operational and safety benefits as traffic volumes become significant.



Mini Roundabouts: Roundabout type characterized by a small diameter and traversable central island; offers most of the benefits of single-lane roundabouts with added benefit of a smaller footprint; best suited to lower-speed environments and where environmental constraints preclude use of a larger roundabout with a raised central island. Mini-roundabouts are emerging in U.S. in states including MD, MI and GA.



Single-Lane Roundabouts: Form of circular intersection in which traffic travels counterclockwise around a central island and in which entering traffic must yield to circulating traffic. Circulating traffic has priority with entries controlled by yield. Geometry slows all traffic into and thru the roundabout. At a 4-leg roundabout there are 8 baseline conflict points.





Multilane Roundabouts: Share same circulatory travel and yield-at-entry in single-lane roundabouts, but include multiple entry and circulatory lanes for one or more approaches that must accommodate vehicles traveling side by side. Important design features include proper entry path alignment and geometry, signing and marking that allows entry to exit paths without forcing a lane change in the circle.

#### Signalized At-Grade Intersections



Signalized Intersection: The most common type of signalized intersection with high driver familiarity. Signal could be simple two-phase or more complex 8-phase to serve vehicular demand. Left turns can be permitted or protected (or combination of both). At a conventional 4-leg intersection there are 32 baseline conflict points.



Median U-Turn: Left turn movements otherwise occurring at the main intersection are made via U-turns in the median, preceding or following right turns. U-turns may be only on major roadway or on both major and minor roadways. A conventional MUT has 16 baseline conflict points and has shown significant operational and safety benefits.



Also known as: Indirect Left, Michigan Left, MUT

Signalized RCUT: Similar to the Median U-turn but
features break in cross-street traffic that allows signals on
opposite directions to operate independently. Left turns
can make directly turns onto the minor road but minor
road thru and left turn movements are made using the
directional U-turn crossovers. An RCUT has 14
baseline conflict points (over 3 intersections).

Also known as: Superstreet



Displaced Left-Turn (DLT): Left turn traffic crosses opposing lanes in advance of main intersection and are stored in additional lanes. At main intersection, thru and left turns can be made simultaneously during same signal phase. A full DLT (both routes) has 28 baseline conflict points; a partial DLT (one route) has 30 baseline conflict

Also known as: Continuous Flow Intersection



RIRO w/Downstream U-Turn: Redirects minor street thru & left turn movements as right-turns followed by a U-turn via directional median crossover (+/- 500 feet from main intersection). Major street lefts are also made indirectly, passing the crossing street and using the same U-turn crossovers in the median. Minor street intersections are reduced to right-in/right-out movements making this the safest intersection type.



Unsignalized High-T: Unsignalized 3-leg intersection features raised channelization to separate "top" thru movement from turning lanes at intersection, allowing the through movement to operate continuously. A high-T intersection has 9 baseline conflict points, the same as a conventional 3-leg.

Also known as: "Seagull" intersection



Offset-Tee Intersection: Creates an offset of minor street approaches to form 2 intersections with the major roadway separated by some distance (between 300' and 500'). Through movements on the minor street "jog" using the major street (right-turns followed by left-turns or vice versa). The Offset-T has a total of 18 baseline conflict points (over two intersections).

Also known as: Paired Intersection

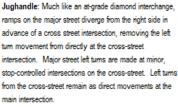


Double Roundabout Interchange: Use of single or dual lane roundabouts at traditional diamond interchange ramp terminals. The use of roundabouts requires only through lanes on the bridge (no turn lane storage lanes) and the elimination of signal control at the ramp terminals. There are a total of 16 baseline conflict points (over two intersections).

Also known as: Teardrop Interchange









Quadrant Roadway: Left turns are removed from the main intersection via an additional roadway in one intersection quadrant. Left-turn movements are routed from the arterial and cross-street (using unique turning paths for each approach) onto the quadrant roadway to complete the left turn movement at the quadrant roadway "minor" T-intersections. A Quadrant Roadway has 28 baseline conflict points (over 3 intersections).



Diverging Diamond Interchange (DDI): All traffic crosses over to left side of road at first ramp terminal intersection before crossing back over at second ramp terminal. Crossover movements allow left turns to be made unopposed. A DDI has a total 14 baseline conflict points (over two intersections) and has shown both operational and safety benefits.

Also known as: Double Crossover Diamond



Single Point Urban Diamond (SPUI): Free-flow major street thru movements are provided by creating a separate, signalized intersection of major street turning movements with the cross-street on a separate grade, creating an intersection either under or over the priority thru roadway. Right turns are made at unsignalized ramps separated from the main intersection.