

14. Transformation of charge+current 4-vector field derived from Electromagnetic 8-vector field \mathbf{F} in $Cl_{3,0}(\mathbb{R})$

(Proof that $\rho + \mathbf{J} = \nabla^\times \mathbf{F}$ transforms in $Cl_{3,0}(\mathbb{R})$ like 4-vectors using hermitian conjugate formula, for the Nabla operator defined as: $\nabla^\times := d/dt - (d/dx)\mathbf{g} - (d/dy)\mathbf{e} - (d/dz)\mathbf{f}$)

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Summary

This article presents a derivation of the transformation of the electromagnetic charge and current density vector $\mathcal{J} = \rho + \mathbf{J}$, where $\mathcal{J} = \nabla^\times \mathbf{F}$ [note¹] and the electromagnetic Clifford vector field \mathbf{F} (in $Cl_{3,0}(\mathbb{R})$) is assumed to transform under length preserving coordinate change as $\mathbf{F}_2 = \exp(\mathbf{p})^* \mathbf{F}^* (\exp(\mathbf{p}))'$, [note²]. It is also assumed that the 4-vectors such as coordinates $\mathbf{q} = t + \mathbf{g}x + \mathbf{e}y + \mathbf{f}z$ and \mathcal{J} must transform as $\mathcal{J}_2 = \exp(\mathbf{p})^* \mathcal{J}^* \exp(\mathbf{p})^T$ [note³].

Introduction

Clifford Algebraic electromagnetic equation has a form of a 4-dimensional (t,x,y,z) differential operator nabla⁴ applied to the complex electromagnetic field 4-vector $\mathbf{F} = -S - \mathbf{E} - i\mathbf{B}$ [see⁵], that must equal zero. This can be also expressed as

$$\mathbf{F} = \nabla^\dagger \mathbf{a} \quad (\text{eq.1, see [4]})$$

where \mathbf{a} is defined as $\mathbf{a} = \phi + \mathbf{A}$, where ϕ is electric potential and \mathbf{A} is magnetic vector potential.

The Nabla operator that applies to 4-vector potential field \mathbf{a} is defined in [4] as⁶:

$$\nabla^\dagger = d/dt + (d/dx)\mathbf{g} + (d/dy)\mathbf{e} + (d/dz)\mathbf{f}$$

¹ $\nabla^\times := d/dt - (d/dx)\mathbf{g} - (d/dy)\mathbf{e} - (d/dz)\mathbf{f}$ [this form is assumed, to prove that it leads to correct transform for $\mathcal{J} = \nabla^\times \mathbf{F}$]

² (') is quaternion conjugate (example $\mathbf{e}' = -\mathbf{e}$ and $(\mathbf{e}\mathbf{f})' = \mathbf{f}'\mathbf{e}'$) We restrict \mathbf{p} to be a linear combination of base vectors $\{\mathbf{g}, \mathbf{e}, \mathbf{f}, i, j, k\}$ only.

³ (T) is hermitian conjugate (example $\mathbf{e}^T = \mathbf{e}$ and $(\mathbf{e}\mathbf{f})^T = \mathbf{f}^T \mathbf{e}^T$)

⁴ $\nabla = d/dt - \mathbf{g} d/dx - \mathbf{e} d/dy - \mathbf{f} d/dz$, $d/dt + \mathbf{g} d/dx + \mathbf{e} d/dy + \mathbf{f} d/dz$

⁵ \mathbf{F} = generalised EM field tensor = $-S - \mathbf{E} - i\mathbf{B} = -S - E_x\mathbf{g} - E_y\mathbf{e} - E_z\mathbf{f} - i(B_x\mathbf{g} + B_y\mathbf{e} + B_z\mathbf{f})$. The general full form is $\mathbf{F} = -S - \mathbf{E} - i\mathbf{B} + iM$, however, the imaginary scalar component M of the Clifford EM field vector \mathbf{F} must be zero or constant in order to cancel the unobservable magnetic monopole charge density and magnetic monopole current density. With M=0, equation $\nabla \mathbf{F} = 0$ corresponds to the well known Maxwell equation, if we define S as $\rho + \mathbf{J} = \nabla S$.

⁶ Partial derivative operator applies first, then a base vector is right-multiplied to the result. The formula can be better understood if the bases g,e,f are put in the denominators as right-divisions, that is:

$$\nabla^\dagger = d/dt + (d/d(x\mathbf{g})) + (d/d(y\mathbf{e})) + (d/d(z\mathbf{f}))$$

Derivation of transform of \mathcal{J}

This assumes that \mathcal{J} is a derivative of some Clifford field \mathbf{F} that transforms using a formula containing quaternion conjugation). The derivation will be split in two cases: (1) Lorentz transform and (2) 3D Rotation.

1) Lorentz transform of \mathcal{J}

Let us take an arbitrary Lorentz transform generator vector \mathbf{u} that is a linear combination of base vectors $\mathbf{e}, \mathbf{f}, \mathbf{g}$. For the sake of consistency with the previously referenced articles [1] etc, it is assumed that base vector \mathbf{g} represents axis x, \mathbf{e} is axis y and \mathbf{f} is axis z.

Without losing the generality of the proof, we can assume that a general generator vector \mathbf{u} (in $\{\mathbf{g}, \mathbf{e}, \mathbf{f}\}$) is aligned with \mathbf{g} (that is there is some real U that $U\mathbf{g} = \mathbf{u}$) The reference frame can always be rotated to align \mathbf{u} with \mathbf{g} (we leave that without proof)

We will indicate the transformed vectors or coordinates with the subscript 2.

The time-space 4-vector $\mathbf{q} = t + \mathbf{g}x + \mathbf{e}y + \mathbf{f}z$ transform as

$$\mathbf{q}_2 = \exp(\mathbf{u}) \mathbf{q} \exp(\mathbf{u})$$

$$\begin{aligned} \mathbf{q}_2 = \exp(\mathbf{u}) \mathbf{q} \exp(\mathbf{u}) &= \exp(2U)t + \exp(2U)x + \mathbf{e}y + \mathbf{f}z = & [\text{note}^7] \\ & t^* \cosh 2U + x^* \sinh 2U + & // t_2 \\ & x^* \cosh 2U \mathbf{g} + t^* \sinh 2U \mathbf{g} + & // x_2 \mathbf{g} \\ & \mathbf{e}y + & // y_2 \mathbf{e} \\ & \mathbf{f}z & // z_2 \mathbf{f} \end{aligned}$$

$$(\text{where } U := \mathbf{u}/\mathbf{g})$$

therefore:

$$t_2 = t^* \cosh 2U + x^* \sinh 2U$$

$$x_2 = x^* \cosh 2U + t^* \sinh 2U$$

$$y_2 = y$$

$$z_2 = z$$

We will transform $\mathcal{J} = \nabla^* \mathbf{F} \leftarrow \mathcal{J}_2 = \nabla^* \mathbf{F}_2$ in reverse, starting with the formula :

$$\mathcal{J} = \nabla^* \mathbf{F} = d\mathbf{F}/dt - d\mathbf{F}/dx \mathbf{g} - d\mathbf{F}/dy \mathbf{e} - d\mathbf{F}/dz \mathbf{f}$$

and evaluating the inner terms.

⁷ We use the following property of exponential function: $\exp(\mathbf{g}U) \mathbf{g} = \mathbf{g} \exp(\mathbf{g}U)$, For perpendicular vectors (i.e. for anti-commuting vectors), for example \mathbf{g} and \mathbf{e} it follows $\exp(\mathbf{g}U) \mathbf{e} = \mathbf{e} \exp(-\mathbf{g}U)$

$$d\mathbf{F}/dt = (d\mathbf{F}/dt_2)*(dt_2/dt) + (d\mathbf{F}/dx_2)*(dx_2/dt) + (d\mathbf{F}/dy_2)*(dy_2/dt) + (d\mathbf{F}/dz_2)*(dz_2/dt) = \\ (d\mathbf{F}/dt_2)*(\cosh 2U) + (d\mathbf{F}/dx_2)*(\sinh 2U)$$

$$d\mathbf{F}/dx = (d\mathbf{F}/dt_2)*(dt_2/dx) + (d\mathbf{F}/dx_2)*(dx_2/dx) + (d\mathbf{F}/dy_2)*(dy_2/dx) + (d\mathbf{F}/dz_2)*(dz_2/dx) = \\ (d\mathbf{F}/dt_2)*(\sinh 2U) + (d\mathbf{F}/dx_2)*(\cosh 2U)$$

$$d\mathbf{F}/dy = (d\mathbf{F}/dt_2)*(dt_2/dy) + (d\mathbf{F}/dx_2)*(dx_2/dy) + (d\mathbf{F}/dy_2)*(dy_2/dy) + (d\mathbf{F}/dz_2)*(dz_2/dy) = (d\mathbf{F}/dy_2) \\ d\mathbf{F}/dz = (d\mathbf{F}/dt_2)*(dt_2/dz) + (d\mathbf{F}/dx_2)*(dx_2/dz) + (d\mathbf{F}/dy_2)*(dy_2/dz) + (d\mathbf{F}/dz_2)*(dz_2/dz) = (d\mathbf{F}/dz_2)$$

Now, we will substitute the \mathbf{F} expressed in terms of the reverse transformed \mathbf{F}_2 into the above formulae, that is: $\mathbf{F} = \exp(-\mathbf{u}) \mathbf{F}_2 \exp(+\mathbf{u})$. This will yield:

$$\begin{aligned} \mathcal{J} = \nabla^* \mathbf{F} &= \exp(-\mathbf{u}) * (d\mathbf{F}_2/dt_2)*\cosh 2U + (d\mathbf{F}_2/dx_2)*\sinh 2U)*\exp(+\mathbf{u}) + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dt_2)*\sinh 2U + (d\mathbf{F}_2/dx_2)*\cosh 2U)*\exp(+\mathbf{u}) * \mathbf{g} + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dy_2)*\exp(+\mathbf{u}) * \mathbf{e} + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dz_2)*\exp(+\mathbf{u}) * \mathbf{f} \\ &= \\ &\quad \exp(-\mathbf{u}) * (d\mathbf{F}_2/dt_2)*(\cosh 2U - \sinh 2U * \mathbf{g}) + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dx_2)*(\cosh 2U - \sinh 2U * \mathbf{g}) * \mathbf{g} * \exp(+\mathbf{u}) + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dy_2) * \mathbf{e} * \exp(-\mathbf{u}) + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dz_2) * \mathbf{f} * \exp(-\mathbf{u}) \\ &= \\ &\quad \exp(-\mathbf{u}) * (d\mathbf{F}_2/dt_2) * \exp(-2\mathbf{u}) * \exp(+\mathbf{u}) + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dx_2) * \mathbf{g} * \exp(-2\mathbf{u}) * \exp(+\mathbf{u}) + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dy_2) * \mathbf{e} * \exp(-\mathbf{u}) + \\ &\quad -\exp(-\mathbf{u}) * (d\mathbf{F}_2/dz_2) * \mathbf{f} * \exp(-\mathbf{u}) \\ &= \exp(-\mathbf{u}) * (d\mathbf{F}_2/dt_2) + (d\mathbf{F}_2/dx_2) \mathbf{g} + (d\mathbf{F}_2/dy_2) \mathbf{e} + (d\mathbf{F}_2/dz_2) \mathbf{f} * \exp(-\mathbf{u}) = \\ &= \exp(-\mathbf{u}) * (\nabla^* \mathbf{F}_2) * \exp(-\mathbf{u}) \\ &= \\ &\quad \exp(-\mathbf{u}) * (\mathcal{J}_2) * \exp(-\mathbf{u}) \end{aligned}$$

therefore, finally:

$$\mathcal{J}_2 = \exp(\mathbf{u}) * (\mathcal{J}) * \exp(\mathbf{u})$$

Therefore, Lorentz transform of \mathcal{J} follows 4-vector transform and is consistent with the hermitian conjugate formula.

2) Rotation transform of \mathcal{J} . [note⁸]

We take as previously, a generator vector \mathbf{v} aligned with the base vector \mathbf{g} (x axis), except this time \mathbf{v} has imaginary coefficient. $\mathbf{v} = i V \mathbf{g}$ where V is a real number and i is imaginary unit (also $i = \mathbf{e}\mathbf{f}\mathbf{g}$)

$$\begin{aligned}
 \mathbf{q}_2 &= \exp(\mathbf{v}) \mathbf{q} \exp(-\mathbf{v}) \\
 \mathbf{q}_2 &= \exp(\mathbf{v}) \mathbf{q} \exp(-\mathbf{v}) = t + \mathbf{g}x + \exp(2\mathbf{v})\mathbf{e}y + \exp(2\mathbf{v})\mathbf{f}z = \quad [\text{note}^9] \\
 &\quad t + \\
 &\quad \mathbf{g}x + \\
 &\quad \mathbf{e}y \cos(2V) - \mathbf{f}y \sin(2V) + \\
 &\quad \mathbf{f}z \cos(2V) + \mathbf{e}z \sin(2V) \\
 &= \\
 &\quad t + \quad \quad \quad // t_2 \\
 &\quad \mathbf{g}x + \quad \quad \quad // x_2 \mathbf{g} \\
 &\quad \mathbf{e}y \cos(2V) + \mathbf{e}z \sin(2V) + \quad // y_2 \mathbf{e} \\
 &\quad \mathbf{f}z \cos(2V) - \mathbf{f}y \sin(2V) \quad // z_2 \mathbf{f}
 \end{aligned}$$

therefore:

$$\begin{aligned}
 t_2 &= t \\
 x_2 &= x \\
 y_2 &= y \cos(2V) + z \sin(2V) \\
 z_2 &= z \cos(2V) - y \sin(2V)
 \end{aligned}$$

We will transform now (in reverse) the $\mathcal{J} = \nabla \mathbf{F}$:

$$\mathcal{J} = \nabla \mathbf{F} = d\mathbf{F}/dt - (d\mathbf{F}/dx)\mathbf{g} - (d\mathbf{F}/dy)\mathbf{e} - (d\mathbf{F}/dz)\mathbf{f}$$

$$\begin{aligned}
 d\mathbf{F}/dt &= (d\mathbf{F}/dt_2)(dt_2/dt) + (d\mathbf{F}/dx_2)(dx_2/dt) + (d\mathbf{F}/dy_2)(dy_2/dt) + (d\mathbf{F}/dz_2)(dz_2/dt) = (d\mathbf{F}/dt_2) \\
 d\mathbf{F}/dx &= (d\mathbf{F}/dt_2)(dt_2/dx) + (d\mathbf{F}/dx_2)(dx_2/dx) + (d\mathbf{F}/dy_2)(dy_2/dx) + (d\mathbf{F}/dz_2)(dz_2/dx) = (d\mathbf{F}/dx_2) \\
 d\mathbf{F}/dy &= (d\mathbf{F}/dt_2)(dt_2/dy) + (d\mathbf{F}/dx_2)(dx_2/dy) + (d\mathbf{F}/dy_2)(dy_2/dy) + (d\mathbf{F}/dz_2)(dz_2/dy) = \\
 &\quad (d\mathbf{F}/dy_2)(\cos 2V) - (d\mathbf{F}/dz_2)(\sin 2V) \\
 d\mathbf{F}/dz &= (d\mathbf{F}/dt_2)(dt_2/dz) + (d\mathbf{F}/dx_2)(dx_2/dz) + (d\mathbf{F}/dy_2)(dy_2/dz) + (d\mathbf{F}/dz_2)(dz_2/dz) = \\
 &\quad (d\mathbf{F}/dz_2)(\cos 2V) + (d\mathbf{F}/dy_2)(\sin 2V)
 \end{aligned}$$

Now, we will substitute the \mathbf{F} expressed in terms of the inverse-transformed \mathbf{F}_2 into the above formulae: $\mathbf{F} = \exp(-\mathbf{v}) \mathbf{F}_2 \exp(\mathbf{v})$. This will yield:

$$\mathcal{J} = \nabla \mathbf{F} = \exp(-\mathbf{v}) (d\mathbf{F}_2/dt_2) \exp(\mathbf{v}) +$$

⁸ This chapter is almost identical as in ref [13], because rotation transform is the same for EM field Clifford 8-vector \mathbf{F} as for 4-vectors such as \mathbf{a} and \mathcal{J} .

⁹ We use the following property of exponential function: $\exp(\mathbf{g}U)\mathbf{g} = \mathbf{g}\exp(\mathbf{g}U)$, For perpendicular vectors (i.e. for anti-commuting vectors), for example \mathbf{g} and \mathbf{e} it follows $\exp(\mathbf{g}U)\mathbf{e} = \mathbf{e}\exp(-\mathbf{g}U)$

$$\begin{aligned}
& -\exp(-\mathbf{v}) * (d\mathbf{F}_2/dx_2)) * \exp(\mathbf{v}) * \mathbf{g} + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dy_2) * (\cos 2V) - (d\mathbf{F}_2/dz_2) * (\sin 2V)) * \exp(\mathbf{v}) * \mathbf{e} + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dz_2) * (\cos 2V) + (d\mathbf{F}_2/dy_2) * (\sin 2V)) * \exp(\mathbf{v}) * \mathbf{f} \\
& = \\
& \exp(-\mathbf{v}) * (d\mathbf{F}_2/dt_2)) * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dx_2)) * \exp(\mathbf{v}) * \mathbf{g} + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dy_2) * (\cos 2V) * \mathbf{e} - (d\mathbf{F}_2/dz_2) * (\sin 2V) * \mathbf{e} + \\
& \quad (d\mathbf{F}_2/dz_2) * (\cos 2V) * \mathbf{f} + (d\mathbf{F}_2/dy_2) * (\sin 2V) * \mathbf{f}) * \exp(-\mathbf{v}) \\
& = \\
& \exp(-\mathbf{v}) * (d\mathbf{F}_2/dt_2)) * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dx_2)) * \mathbf{g} * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dy_2) * (\cos 2V) * \mathbf{e} + (d\mathbf{F}_2/dy_2) * (\sin 2V) * \mathbf{g}(\mathbf{g}\mathbf{f}) + \\
& \quad (d\mathbf{F}_2/dz_2) * (\cos 2V) * \mathbf{f} - (d\mathbf{F}_2/dz_2) * (\sin 2V) * \mathbf{g}(\mathbf{g}\mathbf{e})) * \exp(-\mathbf{v}) \\
& = \\
& \exp(-\mathbf{v}) * (d\mathbf{F}_2/dt_2)) * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dx_2)) * \mathbf{g} * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((\cos 2V) * (d\mathbf{F}_2/dy_2) * \mathbf{e} + (\sin 2V) * (d\mathbf{F}_2/dy_2) * \mathbf{g}(\mathbf{g}\mathbf{f}) + \quad //note^{10} \\
& \quad (\cos 2V) * (d\mathbf{F}_2/dz_2) * \mathbf{f} - (\sin 2V) * (d\mathbf{F}_2/dz_2) * \mathbf{g}(\mathbf{g}\mathbf{e})) * \exp(-\mathbf{v}) \\
& = \\
& \exp(-\mathbf{v}) * (d\mathbf{F}_2/dt_2)) * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dx_2)) * \mathbf{g} * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((\cos 2V) * (d\mathbf{F}_2/dy_2) * \mathbf{e} - (\sin 2V) * (d\mathbf{F}_2/dy_2) * \mathbf{g}(\mathbf{e}\mathbf{i}) + \\
& \quad (\cos 2V) * (d\mathbf{F}_2/dz_2) * \mathbf{f} - (\sin 2V) * (d\mathbf{F}_2/dz_2) * \mathbf{g}(\mathbf{i}\mathbf{f})) * \exp(-\mathbf{v}) \\
& = \\
& \exp(-\mathbf{v}) * (d\mathbf{F}_2/dt_2)) * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dx_2)) * \mathbf{g} * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dy_2) * (\cos 2V - \mathbf{g}\mathbf{i} * \sin 2V) * \mathbf{e} + \\
& \quad (d\mathbf{F}_2/dz_2) * (\cos 2V - \mathbf{g}\mathbf{i} * \sin 2V) * \mathbf{f}) * \exp(-\mathbf{v}) \\
& = \\
& \exp(-\mathbf{v}) * (d\mathbf{F}_2/dt_2)) * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dx_2)) * \mathbf{g} * \exp(\mathbf{v}) + \\
& -\exp(-\mathbf{v}) * ((d\mathbf{F}_2/dy_2) * \exp(-2\mathbf{v}) * \mathbf{e} * + (d\mathbf{F}_2/dz_2) * \exp(-2\mathbf{v}) * \mathbf{f}) * \exp(-\mathbf{v}) \\
& = \\
& \exp(-\mathbf{v}) * (d\mathbf{F}_2/dt_2)) * \exp(\mathbf{v}) + \\
& \exp(-\mathbf{v}) * (- (d\mathbf{F}_2/dx_2)) * \mathbf{g} * \exp(\mathbf{v}) + \\
& \exp(-\mathbf{v}) * (- (d\mathbf{F}_2/dy_2) * \mathbf{e} * \exp(+2\mathbf{v}) - (d\mathbf{F}_2/dz_2) * \mathbf{f} * \exp(+2\mathbf{v})) * \exp(-\mathbf{v}) = \\
& \exp(-\mathbf{v}) * ((d\mathbf{F}_2/dt_2)) - (d\mathbf{F}_2/dx_2)) * \mathbf{g} - (d\mathbf{F}_2/dy_2) * \mathbf{e} - (d\mathbf{F}_2/dz_2) * \mathbf{f}) * \exp(+\mathbf{v}) \\
& = \exp(-\mathbf{v}) * (\nabla^x_2 \mathbf{F}_2) * \exp(\mathbf{v}) \\
& = \exp(-\mathbf{v}) * (\mathcal{J}_2) * \exp(+\mathbf{v}) \\
& \text{Finally}
\end{aligned}$$

¹⁰ $\mathbf{g}\mathbf{f} = -\mathbf{f}\mathbf{g} = -\mathbf{e}\mathbf{e}\mathbf{f}\mathbf{g} = -\mathbf{e}\mathbf{i}$ and $\mathbf{g}\mathbf{e} = \mathbf{g}\mathbf{e}\mathbf{f}\mathbf{f} = \mathbf{e}\mathbf{f}\mathbf{g}\mathbf{f} = \mathbf{i}\mathbf{f}$

$$\mathcal{J}_2 = \exp(+\mathbf{v})^*(\mathcal{J})\exp(-\mathbf{v})$$

Conclusion

In a general case, we can combine the \mathbf{u} and \mathbf{v} cases in one formula that employs the Hermitian conjugate $(\)^T$ [note¹¹]

$$\mathcal{J}_2 = \exp(\mathbf{p})^*(\mathcal{J})\exp(\mathbf{p})^T$$

References:

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- 6) "Standard model physics from an algebra?" by C. Furey
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<https://arxiv.org/pdf/1611.09182.pdf>

¹¹ $\exp(\mathbf{p}) := \exp(\mathbf{u})\exp(\mathbf{v})$, and $\exp(\mathbf{u})\exp(\mathbf{v})' = \exp(\mathbf{v}')\exp(\mathbf{u}')$

13) Proof that EM Clifford 8-vector field F transforms in $Cl_{3,0}(R)$ differently, using quaternion conjugate formula, unlike Clifford 4-vectors transforming using hermitian conjugate formula.
https://docs.google.com/document/d/1e37GgeSA9JOr9nNNRrosEGmPmlhhJX1dBQzuvS8B_04/edit?usp=sharing