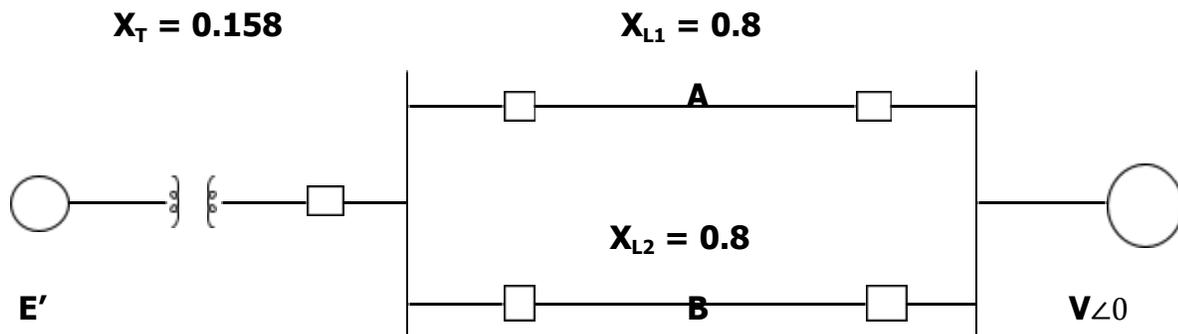


## EXPERIMENT NO.1

**AIM:** To determine the critical clearing angle, critical clearing time for the system shown in Fig.1 when a 3 phase fault occurs at A, which when cleared leaves both lines intact.

Verify the results by MATLAB command and plot the power angle curve.

The system consists of a 60Hz synchronous generator which has a transient reactance of 0.2 pu and an inertia constant of 5.66 MJ/MVA. It is connected to an infinite bus through a transformer and a double circuit transmission line as shown in Fig.8. Resistances & Reactances are expressed on a common MVA base & marked on the diagram. The generator is delivering a real power of 0.77 pu to bus bar 1. The infinite bus voltage is 1.0 pu, the generator excitation is 1.25 pu.



**Fig. 1**

(i) **By Manual Calculation:**

Max Power that can be transformed  $P_{\max} = |E| |V| / X$

Here  $X = j 0.2 + j 0.158 + (j0.8//j0.8) = j0.758$

$$|E| = 1.25$$

$$|V| = 1.0$$

$$P_{\max} = 1.25 * 1.0 / 0.758 = 1.649$$

$$P_M = P_{\max} \sin \delta_0 = 1.65 \sin \delta_0$$

$$0.77 = 1.65 \sin \delta_0 = 27.836 \text{ or } 0.48558 \text{ rad}$$

The power angle will be same before and after removed of fault because lines are intact after the fault is cleared.

$$\delta_{\max} = 180 - \delta_0 = 180 - 27.836 = 152.164 \text{ or } 2.6544 \text{ rad}$$

Since the 3 phase fault is at the beginning of transmission line, the power transfer will be zero.

If we compare

$$P_M = P_{\max} \sin \delta_0 \quad \text{in healthy condition}$$

$$P_M = r_1 P_{\max} \sin \delta_0 \quad \text{in faulty condition}$$

$$P_M = r_2 P_{\max} \sin \delta_0 \quad \text{after fault is cleared}$$

$$\text{Then } r_1 = 0, \quad r_2 = 1$$

Now the critical clearing angle

$$\begin{aligned} \delta_c &= \cos^{-1} \left[ \frac{(\delta_m - \delta_0) \sin \delta_0 - r_1 \cos \delta_0 + r_2 \cos \delta_m}{r_2 - r_1} \right] \\ &= \cos^{-1} \left[ \frac{(2.6544 - 0.48558) * 0.46104 - 0 + 1 * (0.88426)}{1 - 0} \right] \\ &= \cos^{-1} 0.128428 = 82.62^\circ \end{aligned}$$

$$\begin{aligned} \text{Critical clearing time} &= \sqrt{[2H(\delta_c - \delta_0) / \pi f P_M]} \\ &= \sqrt{[2 * 5.66(1.44126 - 0.4/8558) / 3.14 * 60 * 0.77]} \\ &= 0.273 \text{ sec} \end{aligned}$$

### **MATLAB Command**

```
Pm=0.77;E=1.25;V=1.0;  
X1=0.758; X2=inf; X3=0.758;  
eacfault(Pm,E,V,X1,X2,X3)
```

### **Result:**

For this case  $t_c$  can be found from analytical formula.

To find  $t_c$  enter Inertia Constant H, (or 0 to skip)  $H = 5.66$

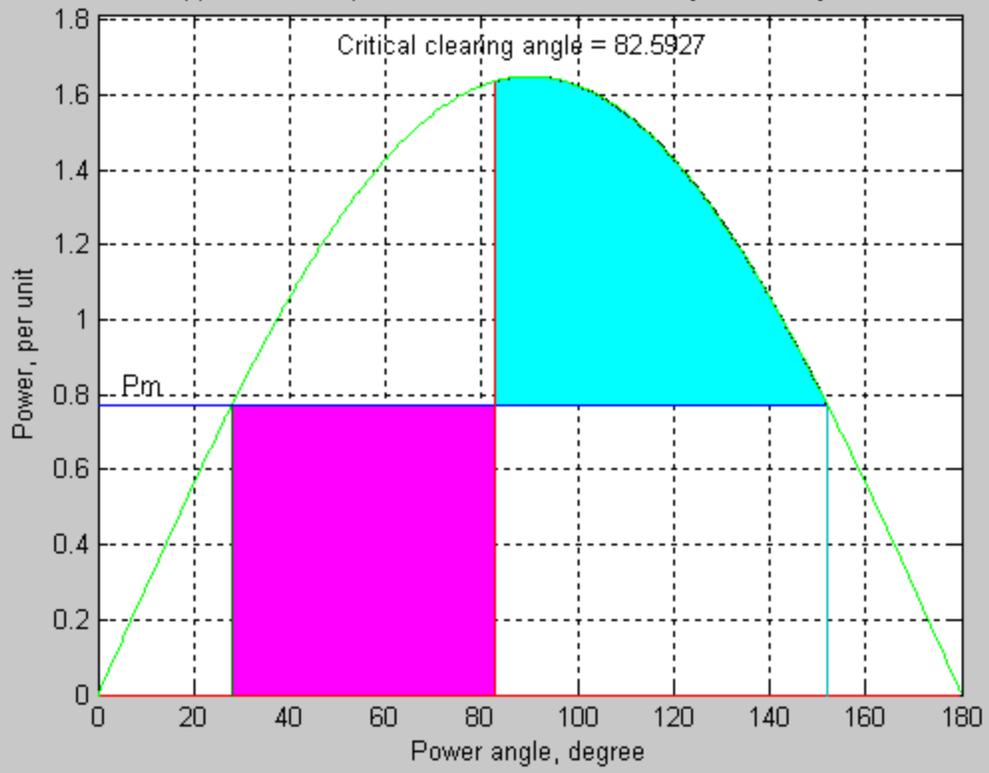
Initial power angle = 27.835

Maximum angle swing = 152.165

Critical clearing angle = 82.593

Critical clearing time = 0.273 sec.

Application of equal area criterion to a critically cleared system

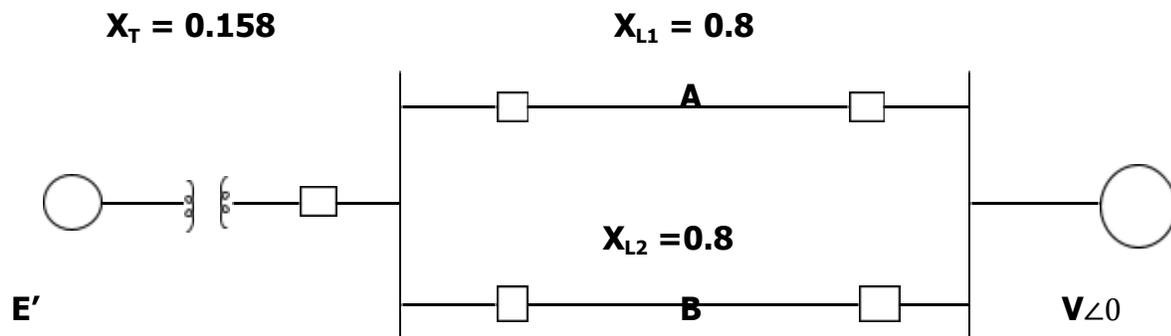


## EXPERIMENT NO. 2

**AIM:** To determine the critical clearing angle, critical clearing time for the system shown in Fig. 2 when a 3 phase fault occurs at the middle of the one line (line B) which when cleared isolated the faulted line.

Verify the results by MATLAB command and display the power angle curve.

The system consists of a 60Hz synchronous generator which has a transient reactance of 0.2 pu and an inertia constant of 5.66 MJ/MVA. It is connected to an infinite bus through a transformer and a double circuit transmission line as shown in Fig.9. Resistances & Reactances are expressed on a common MVA base & marked on the diagram. The generator is delivering a real power of 0.77 pu to bus bar 1. The infinite bus voltage is 1.0 pu, the generator excitation is 1.25 pu.



**Fig. 2**

(i) **By Manual Calculation:**

Under healthy condition  $X_1 = j0.2 + j0.158 + j0.8/2 = j0.758$

Under faulty condition  $X_2 = (j0.358*j0.8 + j0.358*j0.4 + j0.8*j0.4)/j0.4 = j1.874$

When fault is cleared  $X_3 = j0.2 + j0.158 + j0.8 = j1.158$

POWER TRANSFER:

Under healthy condition  $P_{\max} = |E| |V| / X_1 = 1.25*1/0.758 = 1.649$

$$P_e = P_{\max} \sin \delta_0$$

$$0.77 = 1.649 \sin \delta_0$$

$$\delta_0 = 27.836 \text{ or } 0.48558 \text{ rad}$$

Under faulty condition  $P_{\max1} = |E| |V| / X_2 = r_1 P_{\max}$

$$1.25*1/1.874 = r_1 * 1.649$$

$$r_1 = 0.4045$$

When fault is cleared and faulty line is removed

$$P_{\max2} = |E| |V| / X_3 = r_2 P_{\max}$$

$$1.25*1/1.158 = r_2 * 1.649$$

$$r_2 = 0.6546$$

$$\delta_m = 180 - \sin^{-1}[\sin \delta / r_2]$$

$$= 180 - \sin^{-1}[\sin 27.836 / 0.6546]$$

$$= 134.4939^\circ$$

$$\delta_c = \cos^{-1}[\{(\delta_m - \delta_0) \sin \delta_0 - r_1 \cos \delta_0 + r_2 \cos \delta_m\} / (r_2 - r_1)]$$

$$= \cos^{-1}[\{(2.3461 - 0.48558) * 0.46104 - 0.4045 \cos 27.836 + 0.6546 * \cos 134.4939\} / (0.6546 - 0.4045)]$$

$$= 77.916^\circ$$

**(ii) MATLAB Command**

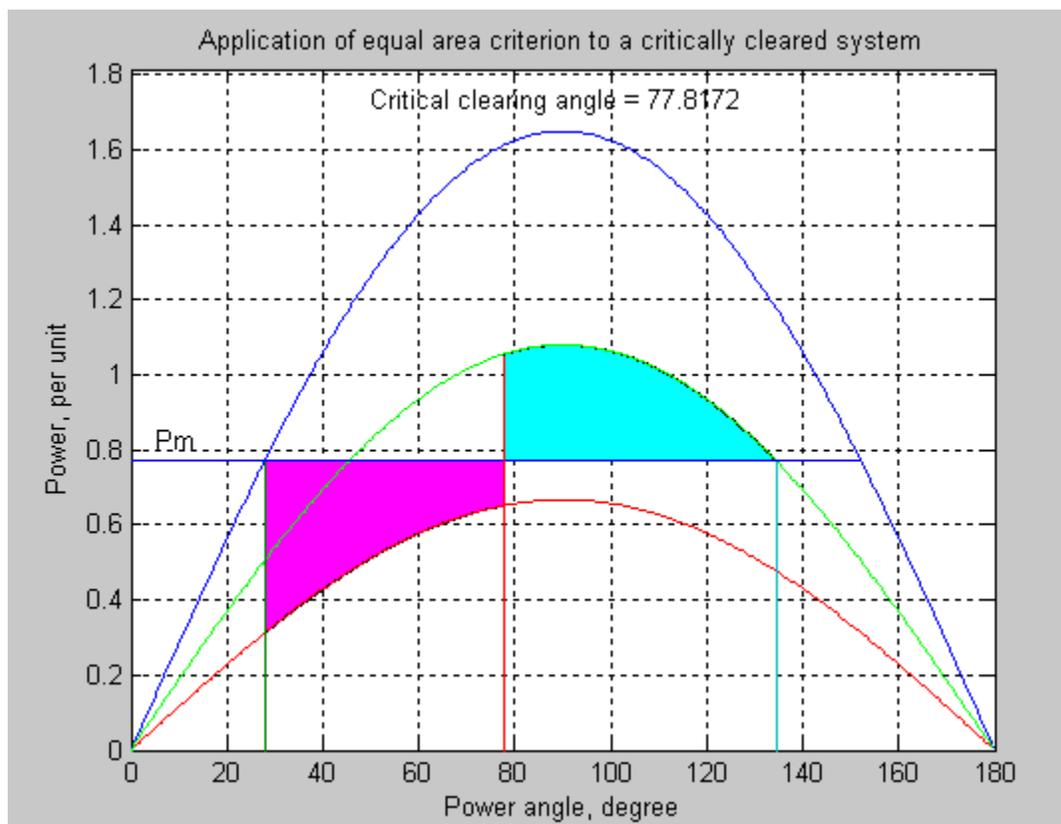
```
Pm=0.77;E=1.25;V=1.0;  
X1=0.758; X2=1.874; X3=1.158;  
eacfault(Pm,E,V,X1,X2,X3)
```

**Result:**

Initial power angle = 27.835

Maximum angle swing = 134.494

Critical clearing angle = 77.817



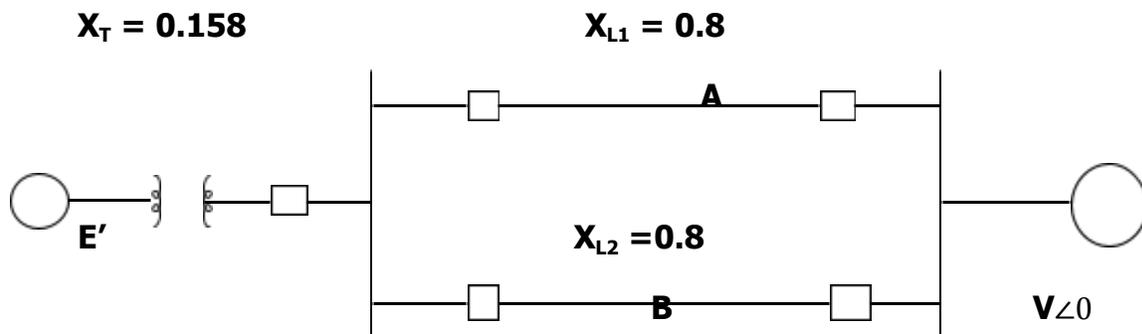
## EXPERIMENT NO.3

**AIM:** To obtain the swing curve for the system shown in Fig.3 by using Modified Euler's method when a 3 phase fault occurs at the middle of the one line and is cleared by isolating the faulted line. Obtain the numerical solution for 1.5 sec for a step size  $\Delta t = 0.01$  sec when fault is cleared in

- i) 0.2 sec.
- ii) 0.3 sec.
- iii) 0.4 sec.

Also draw the flow chart of Euler's and Modified Euler's method.

The system consists of a 60Hz synchronous generator which has a transient reactance of 0.2 pu and an inertia constant of 5.66 MJ/MVA. It is connected to an infinite bus through a transformer and a double circuit transmission line as shown in Fig.3. Resistances & Reactances are expressed on a common MVA base & marked on the diagram. The generator is delivering a real power of 0.77 pu to bus bar 1. The infinite bus voltage is 1.0 pu, the generator excitation is 1.25 pu.



**Fig. 3**

(i) **By Manual Calculation:**

Under healthy condition  $X_1 = j0.2+j0.158+j0.8/2=j 0.758$

Under faulty condition  $X_2 =$

$$(j0.358*j0.8+j0.358*j0.4+j0.8*j0.4)/j0.4=j1.874$$

When fault is cleared  $X_3 = j0.2+j0.158+j0.8= j1.158$

POWER TRANSFER:

Under healthy condition  $P_{\max} = |E| |V| / X_1 = 1.25*1/0.758=1.649$

$$P_{1\max} = P_{\max} \sin \delta_0$$

$$0.77 = 1.649 \sin \delta_0$$

$$\delta_0 = 27.836 \text{ or } 0.48558 \text{ rad}$$

$$\begin{aligned} \text{Under faulty condition } P_{2\max1} &= |E| |V| \sin \delta_0 / X_2 \\ &= 1.25*1* \sin \delta / 1.874 \\ &= 0.667 \sin \delta_0 \end{aligned}$$

Thus accelerating power is given by

$$P_a = 0.77 - 0.667 \sin \delta_0$$

Applying the Modified Euler's method, the derivatives at beginning of step

$$[d\delta/dt]_{\Delta\omega=0} = 0 \text{ and}$$

$$[d\Delta\omega/dt]_{\delta_0} = \frac{\pi f P_a}{H} = 3.14*60(0.77 - 0.667 \sin 27.836)/5.66 = 15.271$$

rad/sec<sup>2</sup>

At the end of first step ( $t_1 = 0.01$  sec), the predicted values are

$$\delta_1^p = \delta_r + [d\delta/dt]_{\Delta\omega} * \Delta t = 0.48558 + 0 * 0.01 = 0.48558 \text{ rad} = 27.836^\circ$$

$$\Delta\omega_1^p = \Delta\omega_0 + [d\Delta\omega/dt]_{\delta_0} * \Delta t = 0 + 15.271 * 0.01 = 0.15271 \text{ rad/sec}$$

Using the predicted value of  $\delta_1^p$  and  $\Delta\omega_1^p$ , the derivatives at end of internal are determined by

$$[d\delta/dt]_{\Delta\omega_1^p} = \Delta\omega_1^p = 0.15271 \text{ rad/sec}$$

$$[d\Delta\omega/dt]_{\delta_1^p} = 3.14*60(0.77 - 0.667 \sin 27.836)/5.66 = 15.271 \text{ rad/sec}^2$$

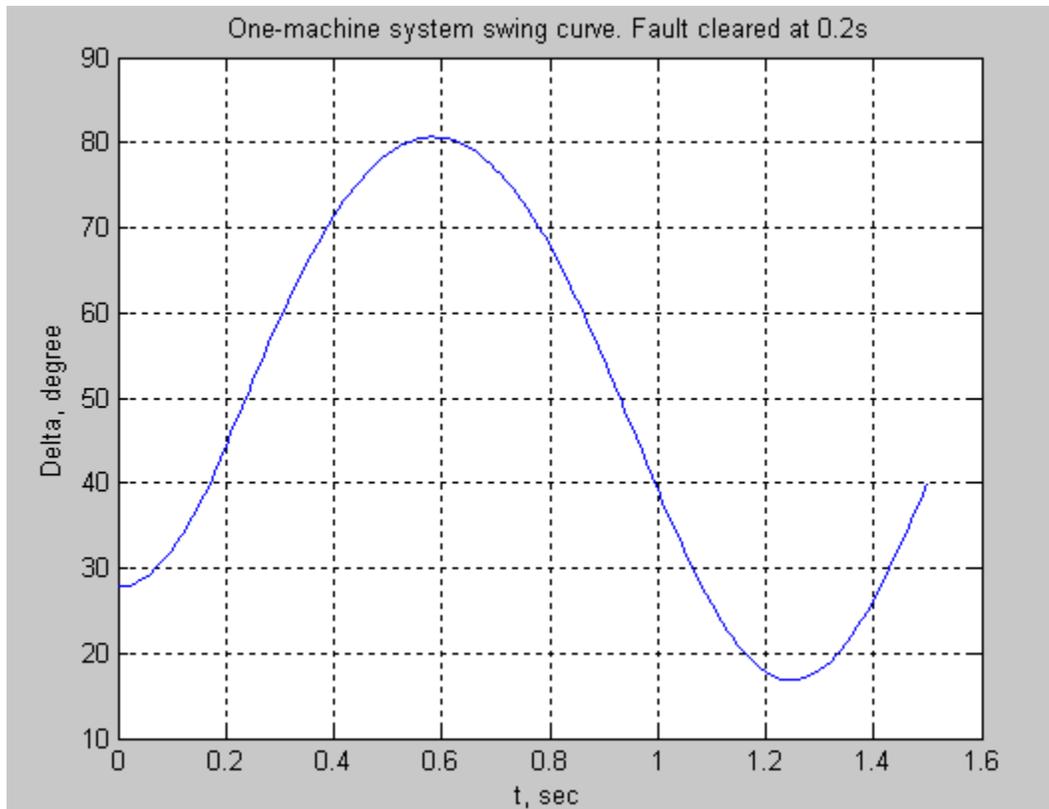
Then the average value of two derivatives is used to find the corrected value

$$\delta_1^c = 0.48558 + (0 + 0.15271) * 0.01 / 2 = 0.48634 \text{ rad}$$

$$\Delta\omega_1^c = 0 + 0.01 * (15.271 + 15.271) / 2 = 0.15271 \text{ rad/sec}$$

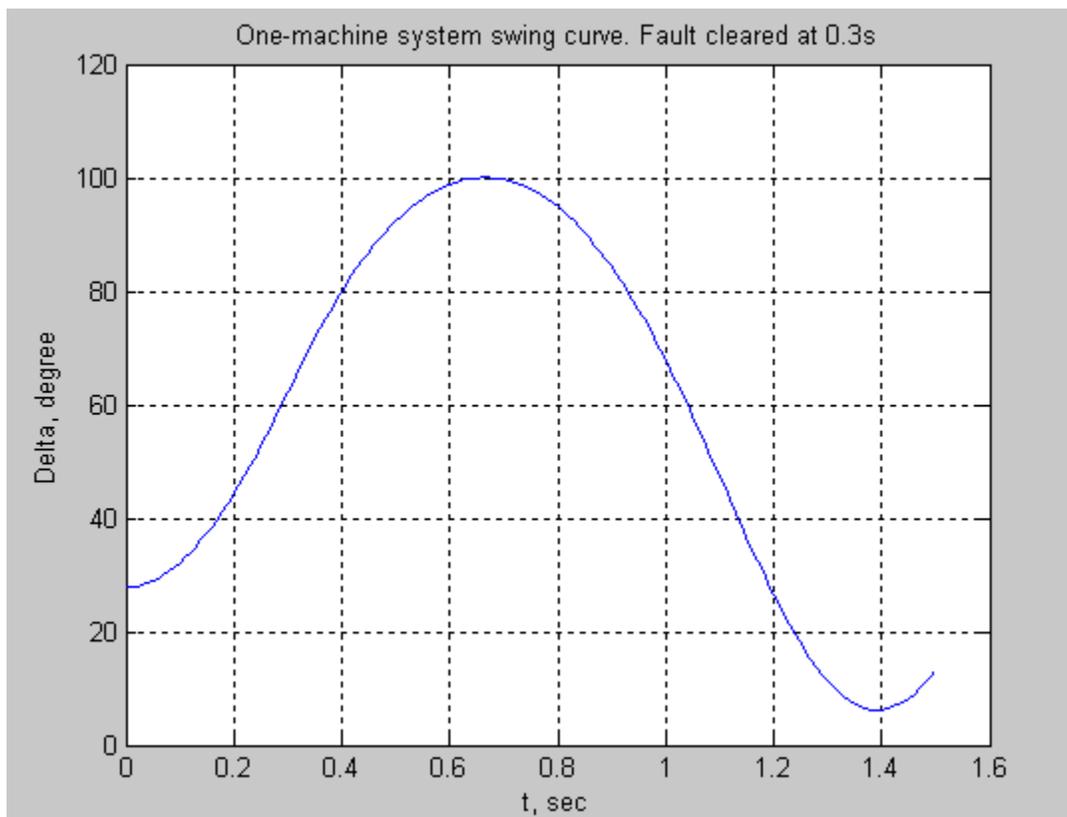
### **MATLAB Command**

```
Pm=0.77;E=1.25;V=1.0;  
X1=0.758; X2=1.874; X3=1.158;  
H=5.66;f=60;tc=0.2;ty=1.5;dt=0.01;  
swingmeu(Pm,E,V,X1,X2,X3,H,f, tc, ty,dt)
```



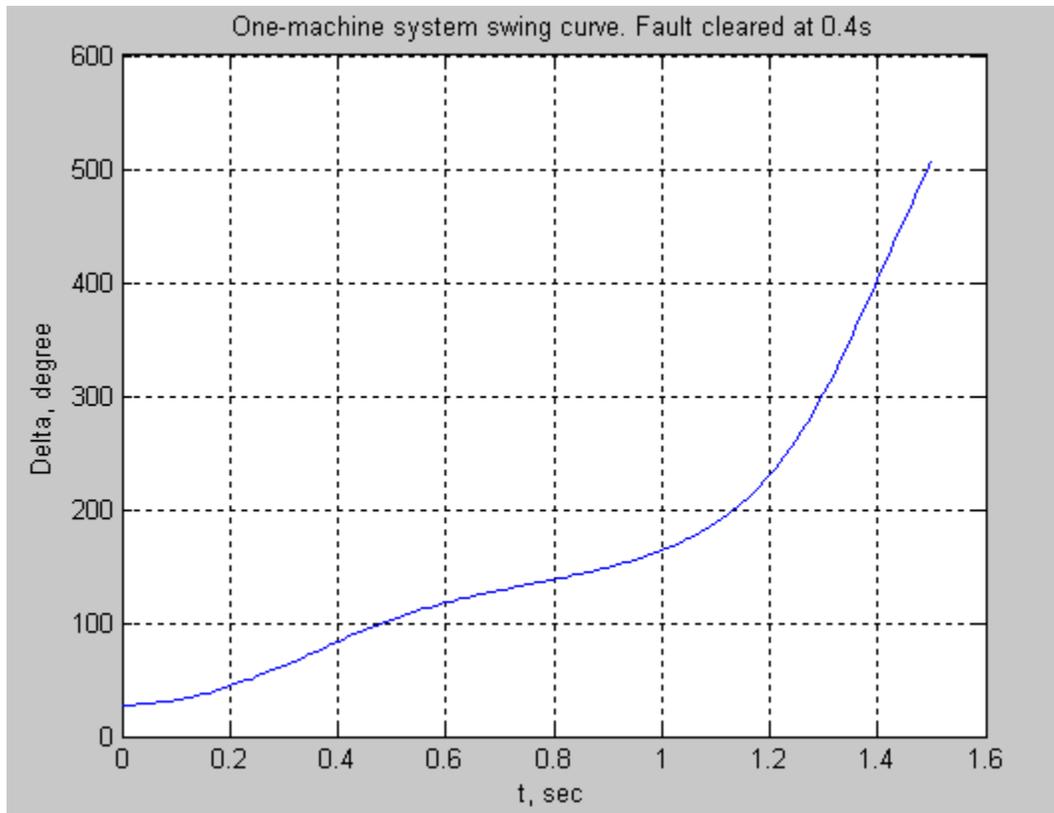
## **MATLAB Command**

```
Pm=0.77;E=1.25;V=1.0;  
X1=0.758; X2=1.874; X3=1.158;  
H=5.66;f=60;tc=0.3;ty=1.5;dt=0.01;  
swingmeu(Pm,E,V,X1,X2,X3,H,f, tc, ty,dt)
```



## MATLAB Command

```
Pm=0.77;E=1.25;V=1.0;  
X1=0.758; X2=1.874; X3=1.158;  
H=5.66;f=60;tc=0.4;ty=1.5;dt=0.01;  
swingmeu(Pm,E,V,X1,X2,X3,H,f, tc, ty,dt)
```



Fault is cleared at 0.400 Sec.			0.4800	99.8311	3.1352	0.9900	162.0747	3.0685
time	delta	Dw	0.4900	101.5994	3.0384	1.0000	163.8746	3.2196
s	degrees	rad/s	0.5000	103.3129	2.9439	1.0100	165.7642	3.3818
0	27.8351	0	0.5100	104.9729	2.8518	1.0200	167.7499	3.5557
0.0100	27.8788	0.1527	0.5200	106.5808	2.7624	1.0300	169.8388	3.7422
0.0200	28.0100	0.3051	0.5300	108.1383	2.6757	1.0400	172.0382	3.9418
0.0300	28.2284	0.4569	0.5400	109.6470	2.5921	1.0500	174.3559	4.1555
0.0400	28.5336	0.6079	0.5500	111.1086	2.5116	1.0600	176.8002	4.3840
0.0500	28.9249	0.7576	0.5600	112.5250	2.4343	1.0700	179.3797	4.6283
0.0600	29.4017	0.9058	0.5700	113.8981	2.3604	1.0800	182.1039	4.8891
0.0700	29.9629	1.0523	0.5800	115.2299	2.2900	1.0900	184.9824	5.1675
0.0800	30.6075	1.1968	0.5900	116.5222	2.2230	1.1000	188.0255	5.4644
0.0900	31.3343	1.3390	0.6000	117.7772	2.1596	1.1100	191.2442	5.7807
0.1000	32.1419	1.4787	0.6100	118.9969	2.0998	1.1200	194.6499	6.1174
0.1100	33.0287	1.6155	0.6200	120.1834	2.0437	1.1300	198.2544	6.4753
0.1200	33.9931	1.7494	0.6300	121.3388	1.9912	1.1400	202.0702	6.8552
0.1300	35.0333	1.8800	0.6400	122.4652	1.9425	1.1500	206.1101	7.2580
0.1400	36.1474	2.0072	0.6500	123.5647	1.8976	1.1600	210.3874	7.6841
0.1500	37.3334	2.1309	0.6600	124.6396	1.8564	1.1700	214.9156	8.1340
0.1600	38.5892	2.2507	0.6700	125.6920	1.8189	1.1800	219.7085	8.6079
0.1700	39.9125	2.3667	0.6800	126.7240	1.7853	1.1900	224.7797	9.1054
0.1800	41.3012	2.4786	0.6900	127.7378	1.7556	1.2000	230.1427	9.6262
0.1900	42.7527	2.5863	0.7000	128.7357	1.7297	1.2100	235.8107	10.1690
0.2000	44.2649	2.6899	0.7100	129.7199	1.7077	1.2200	241.7957	10.7323
0.2100	45.8351	2.7892	0.7200	130.6925	1.6896	1.2300	248.1091	11.3137
0.2200	47.4610	2.8841	0.7300	131.6560	1.6754	1.2400	254.7604	11.9102
0.2300	49.1400	2.9747	0.7400	132.6124	1.6653	1.2500	261.7572	12.5179
0.2400	50.8698	3.0611	0.7500	133.5642	1.6592	1.2600	269.1048	13.1319
0.2500	52.6477	3.1431	0.7600	134.5137	1.6572	1.2700	276.8053	13.7466
0.2600	54.4714	3.2208	0.7700	135.4633	1.6594	1.2800	284.8573	14.3554
0.2700	56.3385	3.2945	0.7800	136.4153	1.6659	1.2900	293.2553	14.9509
0.2800	58.2466	3.3640	0.7900	137.3722	1.6766	1.3000	301.9896	15.5252
0.2900	60.1934	3.4297	0.8000	138.3366	1.6918	1.3100	311.0458	16.0700
0.3000	62.1767	3.4915	0.8100	139.3109	1.7116	1.3200	320.4043	16.5769
0.3100	64.1944	3.5497	0.8200	140.2979	1.7360	1.3300	330.0413	17.0381
0.3200	66.2444	3.6045	0.8300	141.3003	1.7652	1.3400	339.9283	17.4463
0.3300	68.3248	3.6561	0.8400	142.3207	1.7994	1.3500	350.0331	17.7959
0.3400	70.4339	3.7047	0.8500	143.3622	1.8387	1.3600	360.3207	18.0827
0.3500	72.5701	3.7505	0.8600	144.4277	1.8832	1.3700	370.7542	18.3048
0.3600	74.7317	3.7938	0.8700	145.5203	1.9333	1.3800	381.2963	18.4626
0.3700	76.9174	3.8349	0.8800	146.6431	1.9891	1.3900	391.9107	18.5588
0.3800	79.1261	3.8741	0.8900	147.7997	2.0509	1.4000	402.5631	18.5987
0.3900	81.3568	3.9116	0.9000	148.9933	2.1189	1.4100	413.2232	18.5896
0.4000	83.6085	3.9479	0.9100	150.2278	2.1934	1.4200	423.8652	18.5407
0.4100	85.8416	3.8464	0.9200	151.5069	2.2748	1.4300	434.4692	18.4626
0.4200	88.0162	3.7439	0.9300	152.8346	2.3634	1.4400	445.0217	18.3667
0.4300	90.1319	3.6410	0.9400	154.2151	2.4595	1.4500	455.5160	18.2652
0.4400	92.1885	3.5381	0.9500	155.6529	2.5635	1.4600	465.9521	18.1699
0.4500	94.1862	3.4356	0.9600	157.1527	2.6760	1.4700	476.3371	18.0925
0.4600	96.1254	3.3341	0.9700	158.7194	2.7973	1.4800	486.6845	18.0437
0.4700	98.0068	3.2338	0.9800	160.3583	2.9280	1.4900	497.0137	18.0335
						1.5000	507.3494	18.0704