#### **Phase 4 - Design Validation**

Group 8 - Colin Baker, Kory Pringle

#### **Validation Results**

Based on the results from our FEA simulation in Solidworks, our design is a valid femoral fracture plate as it only slightly fails when the femoral head is instantaneously loaded with 800N of force downward. In the FEA, failure was predicted on the front of the plate around the central screw hole, as well as on the back of the plate, mainly in the upper left portion. It was originally predicted that failure would occur near the central screw hole, because of the lack of support and surface area in that section. This result is consistent with the predictions that were made.

#### FEA vs. Back-of-Envelope Calculations

When comparing our FEA to the Back-of-Envelope Calculations done in Phase 3 of this design there is a major discrepancy in output values. The failure of the fracture plate occurs at the same position on the plate however the maximum shear stress is much higher than our calculations done by hand. The maximum shear stress calculated in the Solidworks is 5502.24 MPa greater than the maximum shear stress found by hand. Based on the FEA calculations done in Solidworks we can determine that there was a mistake in the calculations done by hand causing the value of maximum stress to be much lower than it actually is. Since the Back-of-Envelope Calculations are much different we feel as if we should trust the Solidworks FEA over them. With this being said we are also not 100% confident that there was not an error in the Solidworks FEA.

#### **Design Validation Table - FEA Values (Taken for 800N)**

Measurement	Min Value	Max Value
Stress (Von Mises)	0 MPa	5616 MPa
Displacement in Y	-3.030 mm	1.571 mm
Strain	0	3.658e-03
F.O.S	5.034e-02	3

#### **Path Forward**

Overall, our design had a majority of successful results from our FEA, as well as Back-of-Envelope Calculations. In terms of the actual design itself, it included multiple holes and scallops, as well a long axis channel, therefore creating a small contact area, while also keeping the strength of the plate. During the FEA,

the large majority of plate failure occurred around the front central screw hole, and the back upper left side. This could be due to plate error, however this could also be an error in the program in which the plate may not have been placed in an optimal testing area. Going forward, the amount of screw holes and scallops would likely be kept, as well as the channel down the middle. Future improvements would be as follows:

- Possible new orientation of scallops with screw holes
- Make a design that is more fit to a specific femur
- Threading through screw holes for alignment and more security of plate

To summarize, the design did not have many flaws, and most changes would be made simply if given a specific femur with more in depth measurements to design around.



## **Simulation of Femur-Plate Assembly**

Date: Sunday, April 26, 2020 Designer: Solidworks Study name: Static Analysis type: Static

### Description

No Data

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Model name: Femur-Plate Assembly Current Configuration: Default

Solid Bodies			
Document Name and Reference	Treated As	Volumetric Properties	Document Path/Date Modified
Fillet1	Solid Body	Mass:0.0544994 kg Volume:6.93554e-06 m^3 Density:7,857.99 kg/m^3 Weight:0.534094 N	C:\Users\Cbake\OneDrive\ Desktop\School\Sophomore\ Mech of Solids\Design Project\Plate Design 2.SLDPRT Apr 3 23:12:41 2020

Study Properties		
Study name	Static	
Analysis type	Static	
Mesh type	Mixed Mesh	

Thermal Effect:	On	
Thermal option	Include temperature loads	
Zero strain temperature	298 Kelvin	
Include fluid pressure effects from SOLIDWORKS Flow Simulation	Off	
Solver type	FFEPlus	
Inplane Effect:	Off	
Soft Spring:	Off	
Inertial Relief:	Off	
Incompatible bonding options	Automatic	
Large displacement	Off	
Compute free body forces	On	
Friction	Off	
Use Adaptive Method:	Off	
Result folder	SOLIDWORKS document (C:\Users\Cbake\OneDrive\Desktop\School\Sophomore\Mech of Solids\Design Project)	

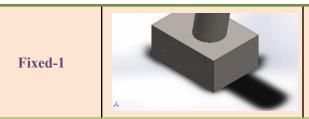
Units		
Unit system: SI (MKS)		
Length/Displacement	mm	
Temperature	Kelvin	

Angular velocity	Rad/sec
Pressure/Stress	N/m^2

**Material Properties** 

Model Reference	Prop		Components
	Name:  Model type: Default failure criterion: Yield strength: Tensile strength: Elastic modulus: Poisson's ratio: Mass density: Shear modulus: Thermal expansion coefficient:	1023 Carbon Steel Sheet (SS) Linear Elastic Isotropic Unknown  2.82685e+08 N/m^2 4.25e+08 N/m^2 2.05e+11 N/m^2 0.29 7,858 kg/m^3 8e+10 N/m^2 1.2e-05 /Kelvin	SolidBody 1(Cut-Extrude6)(Distal Femur-1), SolidBody 1(Fillet1)(Plate Design 2-1), SolidBody 1(Cut-Extrude6)(Proximal Femur-1)
	Curve Dat	ta:N/A	

	Loads and Fixtures		
Ī	Fixture name Fixture Image Fixture Details		



**Entities:** 1 face(s) **Type:** Fixed Geometry

Resultant Forces				
Components	X	Y	Z	Resultant
Reaction force(N)	0	0	0	1e-33
Reaction Moment(N.m)	0	0	0	1e-33

Load name	Load Image	Load Details
Force-1	X.	Entities: 1 face(s)  Type: Apply normal force  Value: 800 N

# Contact Information Contact Contact Image Contact Properties Type: Bonded Components: 1 component(s) Incompatible mesh

Mesh information		
Mesh type Mixed Mesh		
Mesher Used:	Standard mesh	

Automatic Transition:	Off
Include Mesh Auto Loops:	Off
Jacobian points	4 Points
Jacobian check for shell	On
Element Size	0.268274 in
Tolerance	0.0134137 in
Mesh Quality Plot	High
Remesh failed parts with incompatible mesh	Off

Mesh information - Details				
Total Nodes	12784			
Total Elements	6312			
Time to complete mesh(hh;mm;ss):	00:00:03			
Computer name:				
Modification and Pilet Automotion  SOLIDWORNS Educational Product. For Instructional Use Only.				

#### **Resultant Forces**

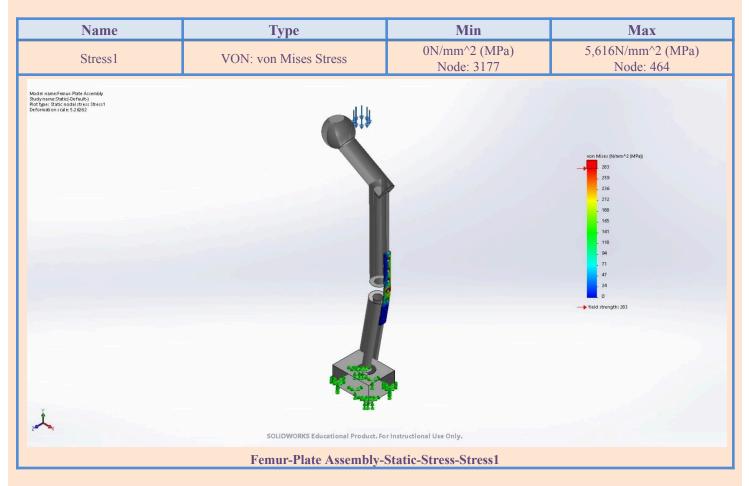
#### **Reaction forces**

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N	-0.0112152	800.007	-0.00187302	800.07

#### **Reaction Moments**

I	Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
	Entire Model	N.m	0	0	0	1e-33

#### **Study Results**



Name	Туре	Min	Max
Displacement1	UY: Y Displacement	-3.030e+00mm Node: 10665	1.571e+00 mm Node: 11648

